Measuring the Fluid Flow Velocity and Its Uncertainty Using Monte Carlo Method and Ultrasonic Technique

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Abstract: One of the most important challenges in fluid mechanics, gas dynamics, and hydraulic machinery fields is measuring the flow velocity with high accuracy. It is more important in large systems; such as thermal power stations, large scale power generations, and combined cycle power plants. The exact estimation of the measurement uncertainty inflow velocity is extremely important in evaluating the accuracy of the measurement. This work describes the problem of estimating measurement uncertainty when there are two or more dominant components of the uncertainty budget. Two methods, analytical and numerical methods are used to study the comparative analysis for the results of determining the expanded uncertainty of measurement using two methods: analytical method and the numerical method. The analytical method uses the law of uncertainty propagation and is based on the estimation of uncertainty values of type A and B, while the numerical technique depends on the evaluation of measured samples by the Monte Carlo method using a random number generator. The aim of this article is to show the Monte Carlo method as an alternative way to determine the distribution of individual components of the measurement uncertainty budget. Also, the measurement of liquid flow velocity by an ultrasonic method has been analyzed, which is commonly used due to high measurement accuracy and non-invasiveness. Due to the complexity of the equation defining the measured flow velocity, determining the measurement uncertainty is not an easy task.

Keywords: Measurement Uncertainty, Monte Carlo Method, Flow Measurement, Ultrasonic Flow Meter.

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Introduction

The exact measuring of a velocity flow in many applications is one of the most important issues in fluid mechanics, gas dynamics, hydraulic machines, and medical device technology [1]. Fluid flow velocity is considered one a key parameters of flow characteristic that should be measured with high accuracy [2]. Determination of the average flow velocity with precise values allows the calculation of the flow rate to create the thermal equilibrium for machines and systems. Flow measurements play a significant role in large systems; such as thermal power stations, large scale power generations, and combined cycle power plants. In many cases, the mass flow rates of steam and cooling water reaches 100 kg/s. With these high flow rates, it is important to ensure a high possible measuring accuracy. Another important problem is the meter assembly and its effect on the operation of the entire installation, since in most measuring methods used, it is necessary to stop the pipeline in order to install the measuring device. Several measuring methods are used to measure the flow velocity and evaluate the uncertainty of the fluid flow-rate or its quantity in the measurements. The ultrasonic flow velocity measurement technique is widely used in industrial and technical measurements due to its high accuracy and non-contact type of flow measurement [3]. Measurement of flow velocity using the Transit-time method with pipeline heads does not require stopping the pipeline and interfering with its geometry. This is a great advantage compared to other commonly used measurement methods, such as the constrictive method. Manufacturers of ultrasonic flow meters declare device accuracy at 2% of the measured value. Achieving device accuracy below 1% of the measured value is only possible for multi-way flow meters [4]. An important condition for maintaining the declared accuracy of measurement is the installation of the flow meter heads while maintaining the straight pipe sections required in the standards [5].

This paper presents the issue of estimating measurement uncertainty when there are two or more dominant components of the uncertainty budget for liquid flow velocity using both the analytical and the Monte Carlo simulation methods. Also, to show that the Monte Carlo method represents an alternative way to determine the distribution of individual components of the measurement uncertainty budget.

2 Implementation of the Measuring Process

Flow meters were used to perform the measurements. The heads of the Endress and Hauser Proline Prosonic Flow 93T ultrasonic flow meter was used. It is designed for temporary monitoring and test measurements with clamp-on sensors. Moreover, conducting verification measurements at existing flow metering points with temperatures ranging from −40 to +170 °C. Generally, the flow meter mounted on a straight section of the pipeline, maintaining the required distance from the elements to avoid disturbance in the flow. The
ultrasonic flowmeter heads were placed on the external surface of the pipeline according to V type method. The heads were assembled by the configuration data from the flowmeter interface. Parameters related to the assembly of the heads and the measuring process are presented in Table 1. Measurements were made in a series of 5 minutes. The averaging time of the speed record was 5 seconds; therefore 60 results were recorded in the measurement series. The measurements were carried out in 2 measurement series for different flow streams, for Reynolds numbers, Re = 35000 and Re = 62000.

<table>
<thead>
<tr>
<th>Parameters for the measurement series: Re=35000</th>
<th>Re=62000</th>
</tr>
</thead>
<tbody>
<tr>
<td>Wall Thickness [mm]</td>
<td>4.0</td>
</tr>
<tr>
<td>Pipe Diameter [mm]</td>
<td>60</td>
</tr>
<tr>
<td>Circumference [mm]</td>
<td>188.5</td>
</tr>
<tr>
<td>Sound Vel. Pipe [m/s]</td>
<td>2400</td>
</tr>
<tr>
<td>Sound Vel. Liq. [m/s]</td>
<td>1461</td>
</tr>
<tr>
<td>Temperature [°C]</td>
<td>12.3</td>
</tr>
<tr>
<td>Sensor Distance [mm]</td>
<td>90.01</td>
</tr>
</tbody>
</table>

### 3.1 Errors In The Process Of Speed Measurement By Ultrasonic Flow Meter

The technical documentation of the Endress - Hauser Prosonic Flow 93T ultrasonic flow meter used during testing to describe the maximum measurement errors at the measuring point as the sum of the error of the measuring device- \( \delta_{\text{dev}} \) and the error of the installation of the ultrasonic heads [17]. Figure 1 shows a photograph of the Endress - Hauser portable ultrasonic flowmeter Prosonic Flow 93T device.
The error measured by this device can be expressed as:

\[ \delta_{dev} = 0.5\% \cdot v_{mes} \pm 7.5 \text{ mm/s} \]  

(1)

\[ \delta_{inst} = 1.5\% \cdot v_{mes} \]  

(2)

The total maximum measurement error at any point of the measurement range, i.e. the maximum error, is given by formula (3):

\[ \delta_{mes} = \delta_{dev} + \delta_{inst} = 2\% \cdot v_{mes} + 7.5 \text{ mm/s} \]  

(3)

For the purpose of further calculations, the limit error \( \delta_{mes} \) was divided into two components \( \delta_{g1} \) and \( \delta_{g2} \).

\[ \delta_{g1} = 2\% \cdot v_{mes} \]  

(4)

\[ \delta_{g2} = 7.5 \text{ mm/s} = 0.0075 \text{ m/s} \]  

(5)

### 3.2 Analytical Method for Determining Measurement Uncertainty

The uncertainty of flow velocity measurement was performed by the use of the ultrasonic method based on GUM standards. The standard uncertainty of speed measurement is the geometric sum of the type A of uncertainty and the type B of uncertainty [18].

\[ u(v) = \sqrt{u_A^2 + u_g^2} \]  

(6)

During the experimental operations, two measuring series of 60 recorded results were made each. The measure of measurement uncertainty of type A is the standard deviation of the mean, determined for \( n = 60 \) measurements. It was assumed that the measurement results are subject to normal probability distribution.

\[ u_A = \sqrt{\frac{\sum_{i=1}^{n=60}(v_{mes} - \overline{v}_{mes})^2}{n(n-1)}} \]  

(7)

Type B uncertainty is the uncertainty of the correction of the ultrasonic flowmeter indication and is expressed by the formula (8). The boundary errors \( \delta_{g1} \) and \( \delta_{g2} \) are subject to a rectangular probability distribution.

\[ u_B = \frac{\delta_{g1}}{\sqrt{3}} + \frac{\delta_{g2}}{\sqrt{3}} = \frac{2\% \cdot v_{mes}}{\sqrt{3}} + \frac{0.0075}{\sqrt{3}} \]  

(8)

Ultimately, the total uncertainty of measurement can be written by (9)

\[ u(v) = \sqrt{u_A^2 + (2\% \cdot v_{mes} \cdot \sqrt{3} + 0.0075 \cdot \sqrt{3})^2} \]  

(9)

The expanded uncertainty of the flow velocity measurement is for the assumed confidence interval \( P = 95\% \). Because the dominant component of total uncertainty is type B uncertainty \( u_B \), so the assumed expansion factor according to [4] is \( k = k_B \cdot p = \sqrt{3} \cdot 0.95 = 1.65 \) [19]. Finally, expanded uncertainty takes the form (10)

\[ U(v) = k \cdot u(v) = 1.65 \cdot u(v) \]  

(10)

The uncertainty budget determined in the above manner for the flow velocity estimates \( v_{mes} = 0.9300 \text{ m/s} \) and \( v_{mes} = 1.7687 \text{ m/s} \) are presented in Table 2 and Table 3.

### 4 Results and Discussion

In order to verify the uncertainty calculations with the analytical method presented in the subsections above, a numerical simulation of the uncertainty budget was performed. For this purpose, the Monte Carlo method was used, generating probability distributions for given input parameters (expected value and uncertainty).
Table 2. Uncertainty budget components determined analytically for Re = 35000.

<table>
<thead>
<tr>
<th>Size x</th>
<th>Size estimated</th>
<th>Variance standard u² (x)</th>
<th>Schedule probability</th>
<th>Sensitivity factor</th>
<th>Share in compound variance</th>
</tr>
</thead>
<tbody>
<tr>
<td>v mes</td>
<td>0.9300</td>
<td>9.5E-07</td>
<td>Normal</td>
<td>1.0000</td>
<td>9.5E-07</td>
</tr>
<tr>
<td>δg1</td>
<td>0.0000</td>
<td>1.2E-04</td>
<td>Rectangular</td>
<td>1.0000</td>
<td>1.2E-04</td>
</tr>
<tr>
<td>δg2</td>
<td>0.0000</td>
<td>1.9E-05</td>
<td>Rectangular</td>
<td>1.0000</td>
<td>1.9E-05</td>
</tr>
</tbody>
</table>

| Standard uncertainty u (v) | 0.0116                |
| Extended uncertainty U (v) | 0.0192                |
| Relative uncertainty δu (v) | 2.06%                 |

Table 3. Uncertainty budget components determined analytically for Re=62000

<table>
<thead>
<tr>
<th>Size x</th>
<th>Size estimated</th>
<th>Variance standard u² (x)</th>
<th>Schedule probability</th>
<th>Sensitivity factor</th>
<th>Share in compound variance</th>
</tr>
</thead>
<tbody>
<tr>
<td>v mes</td>
<td>1.7687</td>
<td>1.8E-06</td>
<td>Normal</td>
<td>1.0000</td>
<td>1.8E-06</td>
</tr>
<tr>
<td>δg1</td>
<td>0.0000</td>
<td>4.2E-04</td>
<td>Rectangular</td>
<td>1.0000</td>
<td>4.2E-04</td>
</tr>
<tr>
<td>δg2</td>
<td>0.0000</td>
<td>1.9E-05</td>
<td>Rectangular</td>
<td>1.0000</td>
<td>1.9E-05</td>
</tr>
</tbody>
</table>

| Standard uncertainty u (v) | 0.0209                  |
| Extended uncertainty U (v) | 0.0345                  |
| Relative uncertainty δu (v) | 1.95%                  |

The Monte Carlo method is often used to simulate the uncertainty budget of measurements of various types [20-22]. The key to simulating the measurement uncertainty budget with the Monte Carlo method is to write the measurement equation. The measurement equation, in the form of velocity value measured with an ultrasonic flow meter together with measurement uncertainty, has the form given in equation (11), such that:

\[ v = \bar{v}_{mes} + \delta g_1 + \delta g_2 \]  

(11)

For the simulation, the values contained in Table 2 and Table 3 were used as input quantities. In order to implement the Monte Carlo method to determine the uncertainty of flow velocity measurement, a calculation sheet was created in MS Excel-Figure 2. The simulation was carried out for 10,000 samples and the same probability distributions for individual quantities were used for the analytical method. Using the Monte Carlo method, the probability density functions were determined, the expected value and the expanded uncertainty value were calculated for the P = 95% confidence interval.

Moreover, the results of the analytical method were obtained and compared with the results of calculations made by the Monte Carlo method. The results of numerical simulation using the Monte Carlo method are presented in Figures 3 and 4. Figure 3 shows the representative frequency distribution for simulated results of the flow velocity. The median and mean values are at 1.7687 m/s with a density of 350 for higher Re=6200. It is with relative uncertainty \( \delta u (v) = 1.95\% \). Figure 4 shows the representative frequency distribution lower Re=3500, the median and mean values are 0.9340 m/s with a density of 400 and relative uncertainty \( \delta u (v) = 2.06\% \). The error of estimation increases as we are going from the right or left of the mean value that coexist in the middle of the chart and separates the lower 50% of the data. The uncertainty is lower for higher Reynolds numbers due to the higher mean velocity in the denominator of percentage ratio.
Fig. 2. A calculation sheet made for estimating the uncertainty budget with the Monte Carlo method.

It can be noticed from figure 2 which represents the calculation sheet made for estimating the uncertainty budget with the Monte Carlo method that the study is carried out on about 10000 sample, the excel sheet calculates the mean, standard deviation, maximum, minimum and then uncertainty. The values of uncertainty in measuring fluid flow velocity are ranged from 0.00134 to 0.0043 at confidence interval of 0.95.
Fig. 3. Histogram from Monte Carlo simulation for the estimation of the measured quantity \( \bar{v}_{mes} = 1.7687 \) m/s for flow of Re=62000

Fig. 4. Histogram from Monte Carlo simulation for the estimation of the measured quantity \( \bar{v}_{mes} = 0.9300 \) m/s for flow of Re=35000

Figures 5 and 6 show the probability density functions for the estimation of the measured quantitates. Figure 5 shows the probability density for the mean velocity of \( \bar{v}_{mes} = 1.7687 \) m/s at Re=62000. As shown in figures, the probability of getting the true value increases as the velocity increases. In figure 5, it grows up at 1.765 m/s to achieve the maximum value with a 100% probability at 1.774 m/s flow velocity. In figure 6, it grows up at 0.927 m/s to achieve the maximum value with a 100% probability at 0.9340 m/s flow velocity. The shape of the distribution of mean velocity was mainly affected by the type of flow and the frequency plotted in figures 7 and 8.

Fig. 5. A numerical cumulative distribution function for an estimate of the measured quantity \( \bar{v}_{mes} = 1.7687 \) m/s and Re=62,000

Fig. 6. A numerical cumulative distribution function for an estimate of the measured quantity \( \bar{v}_{mes} = 0.9300 \) m/s and Re=35,000

Figures 7 and 8 show the frequency density distribution of the simulated numerical values of flow velocity \( V_m \) for both 62,000 and 35,000 Reynolds numbers. Figure 7 and 8 describes the shapes of the mean measurements of stream wise velocities and their fluctuation beyond the grid for relatively higher and lower turbulent flow [23]. It gives an indication about the size of error occurred in measuring the flow speed at each value and how it was far from the true value. As shown in these figures, the average of the two quantities of flow velocity near the center of the layers is the maximum, where the frequency is the highest due to the discontinuous nature of the flow in these regions [24].
It is lower for higher Reynolds numbers, as discussed before. As presented in the figures, the simulations of mean flow velocity shows the frequencies with the smallest level of fluctuations were near the edges [20] and the different inlet stream conditions in a pipe will affect the output flow characteristics and the amount of frequencies [25, 26].

According to the related data listed in Table 4, the expanded uncertainty of variation is much smaller for lower Re (35,000) than the values obtained for higher Re (62,000). Comparing the values presented in Table 4, it must be stated that for both measurement series, the uncertainty values are different and in both cases. The value of the uncertainty determined by the Monte Carlo method is lower than that determined by the analytical method. The relative difference between the two values is 7.7% and 4% respectively for the measurement series made at Reynolds number Re = 35,000 and Re = 62,000. However, this difference is acceptable because the final record of the measurement result (including uncertainty) is made with two significant digits. In the case of a measurement series made with Reynolds number Re = 35,000, the final measurement result was the same for the numerical method of Monte Carlo method: \( v = (0.93 \pm 0.02) \) m/s. For a measurement series made with a Reynolds number Re = 62,000, the results obtained by the analytical and numerical methods should be written equally as \( v = (1.77 \pm 0.04) \) m / s. The final record of the measurement result is nearly the same, despite the differences in the uncertainty values determined by both methods.

Table 4 summarizes the data and results achieved to estimate the velocity mean flow \( v \) and the expanded uncertainty \( U(v) \) as estimated by both; the analytical technique, and the Monte Carlo one. As seen from the results, the measurement uncertainty of the velocity flow by both methods are nearly the same. For Re =35,000, the comparative uncertainties for the analytical method and the Monte Carlo are 0.0192, 0.0208 respectively. For Re =62,000, the values are equal to 0.0345, 0.0360 respectively. According to the related data listed in Table 4, the expanded uncertainty of variation is much smaller for lower Re (35,000) than the values obtained for higher Re (62,000). Comparing the values presented in Table 4, it must be stated that for both measurement series, the uncertainty values are different and in both cases. The value of the uncertainty determined by the Monte Carlo method is lower than that determined by the analytical method. The relative difference between the two values is 7.7% and 4% respectively for the measurement series made at Reynolds number Re = 35,000 and Re = 62,000.

Table 4. Comparison of calculation of measurement uncertainty by analytical and numerical methods.

<table>
<thead>
<tr>
<th>Method</th>
<th>Re=35,000</th>
<th>Re=62,000</th>
</tr>
</thead>
<tbody>
<tr>
<td>Uncertainty determination method</td>
<td>v</td>
<td>U(v)</td>
</tr>
<tr>
<td>Analytical</td>
<td>0.9300</td>
<td>0.0192</td>
</tr>
<tr>
<td>Monte Carlo</td>
<td>0.9299</td>
<td>0.0208</td>
</tr>
</tbody>
</table>

5 Conclusions

Based on the results and comparisons of using two different ways, traditional and Monte Carlo methods of determining measurement uncertainty, the following conclusions can be made:

- Through analyzing the results obtained, it can be stated that the Monte Carlo method can be used to determine measurement uncertainty.
- It enables a graphical representation of the probability distributions of individual variables included in the measurement equation. However, one should remember about the necessity to verify the obtained measurement uncertainty value with the uncertainty value calculated on the basis of types A and B, in accordance with GUM standards.

- In the analyzed calculation example, the final record of the measurement results, with the recommended accuracy of 2 significant digits, is the same for both methods of determining uncertainty.

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