

Employment of Generalized Receiver in DS-CDMA with STBC over Fading Channels: Capacity and Error Probability

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Abstract: - The capacity and error probability of orthogonal space-time block codes (STBCs) are considered for the pulse-amplitude modulation (PAM), phase shift keying (PSK), quadrature-amplitude modulation (QAM) in fading channels. The suggested approach is based on employment of the generalized approach to signal processing in noise over the equivalent scalar additive white Gaussian noise channel with a channel gain proportional to the Frobenius norm of the matrix channel for the STBC. Using this effective channel, the capacity and probability of error expressions are derived for the PSK, PAM, and QAM modulation with space-time block coding. The Rayleigh, Rician and Nakagami fading channels are considered. As an application, these results are extended to obtain the capacity and probability of error for a multiuser direct sequence code-division multiple-access (CDMA) system constructed on the basis of the generalized approach to signal processing in noise employing the space-time block coding.

Key-Words: - Generalized receiver, code-division multiple-access (CDMA), fading channels, phase shift keying, pulse amplitude modulation, quadrature amplitude modulation, Rayleigh channel, Rician channel.

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1 Introduction

The growing demand for high-rate data services through wireless communication channels experienced in recent years motivates the design of multiple antenna wireless communication systems to transmit increase data rates without substantial bandwidth expansion. In particular, the antenna diversity can be used to improve the performance of wireless communication systems such as the code-division multiple-access (CDMA). First presented in [1] for two transmitting antennas and generalized in [2] and [3] for an arbitrary number of transmitting antennas, the orthogonal space-time block coding (STBC) is a remarkable technique which can provide full diversity gain with very low computational complexity.

However, a loss in capacity, characterized by the code rate and the number of receive antennas, is discussed shown in [4] and [5] for an arbitrary channel. Following the analysis in [3]-[5], a characterization based on the equivalent scalar additive white Gaussian noise (AWGN) channel multiplied by a coefficient, which is a function of the Frobenius norm of the channel matrix with multiple antennas, was given in [4] assuming a full code rate. The Shannon and

outage capacity for the scalar AWGN channel were also given.

The Shannon capacity

$$C = W \log_2(1 + SNR), \quad (1)$$

where SNR is the signal-to-noise ratio and W is the channel bandwidth, predicts the channel capacity C for an AWGN channel with continuous-valued inputs and continuous-valued outputs. However, a channel employing the STBC with the pulse-amplitude modulation (PAM), phase shift keying (PSK) or quadrature-amplitude modulation (QAM) has discrete-valued inputs and continuous-valued outputs, which imposes an additional constraint on the capacity calculation.

In this paper, we generalize the effective channel representation in [4] for all rate orthogonal STBCs, including the rate 0.5 STBCs \mathbf{G}_N , $N > 2$ and the rate 0.75 STBCs \mathbf{H}_3 and \mathbf{H}_4 , given in [2]. A new capacity calculation taking into account the constraint of discrete-valued inputs is presented here, as well as the capacity loss incurred by employing STBC.

In [6], an analysis of the bit error probability (BEP) of \mathbf{G}_2 for q -ary PSK was presented for the Rayleigh fading channel using the probability density

function (pdf) of the received signal phase from [7]. However, the *BEP* for *q*-PSK ($q > 4$) is very complex using this approach. In [8], a union bound on the symbol error probability (*SEP*) for the STBC was presented. A general form for the exact pair wise error probability of STBCs was obtained in [9] based on the moment generating function of the Gaussian tail function. In [10], the STBC was applied to a CDMA downlink, and a novel decoding algorithm was presented. In [11], the exact expression for the pair wise error probability in a flat Rayleigh fading channel was derived in terms of the symbol distance between two message vectors for quaternary phase-shift keying (QPSK), 16-QAM, 64-QAM and 256-QAM. In [12], a unified approach to calculate the error rates of linearly modulated signals over generalized fading channels was presented. However, the results of both [11] and [12] are given in an open form that has to be evaluated via numerical integration.

In this paper, we analyze the error probability of STBCs for PAM, PSK, QAM modulated signals as a function of an *SNR* perspective based upon the equivalent scalar channel induced by the STBC. Using the pdf of the *SNR*, the closed form *SEPs* are given for various combinations of modulation and fading channels. Furthermore, these results are extended to a multiuser DS-CDMA system with STBC employing the generalized receiver. Expressions for the capacity and error probability of the DS-CDMA system with STBC are derived and analyzed.

2 Channel Model

2.1 General channel model

The channel model is the same as in [2]-[4]. Consider the wireless communication system with N transmit and M receive antennas. The channel is assumed to be quasistatic with flat fading, which means that the channel parameters are constant within one frame period, but are varied independently between frames. Furthermore, the perfect channel state information is assumed available at the receiver input, but the channel parameters are unknown at the transmitter.

Let T represents the number of time slots used to transmit S symbols. Hence, a general form for the transmission matrix of STBC is given as

$$\mathbf{G} = \begin{pmatrix} g_{11} & g_{21} & \cdots & g_{N1} \\ g_{12} & g_{22} & \cdots & g_{N2} \\ \cdots & \cdots & \cdots & \cdots \\ g_{1T} & g_{2T} & \cdots & g_{NT} \end{pmatrix}, \quad (2)$$

where g_{ij} represent a linear combination of the signal constellation components and their conjugates, and are transmitted simultaneously by the i -th transmit-

ting antenna in the j -th time slot for $i = 1 \dots N$ and $j = 1 \dots T$. Since there are S symbols transmitted over T time slots, the code rate of the STBC is given by

$$R = S/T. \quad (3)$$

It is shown in [2], based on the theory of orthogonal designs, that full rate STBCs exist for any number of transmitting antennas using an arbitrary real constellation such as PAM. For an arbitrary complex constellation such as PSK, QAM, the half rate STBCs exist for any number of transmitting antennas, while full rate STBCs exist only for two transmitting antennas. As specific cases for two, three, and four transmitting antennas, the rate 1, 0.5, and 0.75 STBCs are given in [2], and are denoted as \mathbf{G}_2 , \mathbf{G}_3 , \mathbf{G}_4 , \mathbf{H}_3 , and \mathbf{H}_4 , respectively. At a particular time nT , the received signal corresponding to the n -th input block spanning T time slots takes the form

$$\mathbf{Y}_{nT} = \mathbf{H}\mathbf{G}^T + \mathbf{W}_{nT} \quad (4)$$

where \mathbf{Y}_{nT} is the $M \times T$ matrix; \mathbf{H} is the $M \times N$ fading channel coefficient matrix with the independent identically distributed (i.i.d.) entries modelled as the circular complex Gaussian random variables; \mathbf{G}^T is the transpose of \mathbf{G} with the size $N \times T$, and \mathbf{W}_{nT} is the $M \times N$ receiver noise matrix with the i.i.d. entries modelled as the circular complex Gaussian random variables with zero mean and variance $\sigma_w = \Delta f \times \mathcal{N}_0/2$ in each dimension, where Δf is the bandwidth of linear system at the receiver input and $\mathcal{N}_0/2$ is the AWGN power spectral density.

2.2 Effective scaled AWGN channel

In [4], an equivalent scaled AWGN channel induced by the STBC for the complex constellations was given as

$$\mathbf{y}_{nT} = \|\mathbf{H}\|_F^2 \mathbf{x}_{nT} + \mathbf{w}_{nT}, \quad (5)$$

where \mathbf{y}_{nT} is the $S \times 1$ complex matrix after STBC decoding from the received matrix \mathbf{Y}_{nT} ; \mathbf{x}_{nT} is the input $S \times 1$ complex input matrix with each entry having the energy E_s/N , E_s is the maximum total transmitted energy on the N transmit antennas per symbol time; and \mathbf{w}_{nT} is the complex Gaussian noise with the zero mean and variance $\|\mathbf{H}\|_F^2 \mathcal{N}_0/2$ in each real dimension;

$$\|\mathbf{H}\|_F^2 = \sum_{i=1}^N \sum_{j=1}^M |h_{ij}|^2 \quad (6)$$

is the squared Frobenius norm of \mathbf{H} ; h_{ij} is the channel gain from the i -th transmit antenna to the j -th receive antenna. Taking into account the code rate, the equivalent AWGN scaled channel with STBC is

$$\mathbf{y}_{nT} = (1/R) \|\mathbf{H}\|_F^2 \mathbf{x}_{nT} + \mathbf{w}_{nT}, \quad (7)$$

where \mathbf{w}_{nT} is the complex Gaussian noise with the zero mean and variance given as

$$\text{Var} = (1/2R) \|\mathbf{H}\|_F^2 \mathcal{N}_0 \quad (8)$$

in each real dimension. Therefore, the effective instantaneous SNR denoted as γ_s at the receiver input takes the following form

$$\gamma_s = \frac{E_s}{NR\mathcal{N}_0} \|\mathbf{H}\|_F^2. \quad (9)$$

Let

$$h = \frac{1}{R} \|\mathbf{H}\|_F^2 = \sum_{i=1}^N \sum_{j=1}^M \frac{|h_{ij}|^2}{R}, \quad (10)$$

then the STBC channel model of (7) can be simplified to

$$\mathbf{y}_{nT} = h\mathbf{x}_{nT} + \mathbf{w}_{nT} \quad (11)$$

and γ_s can be written as

$$\gamma_s = \frac{E_s}{N\mathcal{N}_0} h. \quad (12)$$

2.3 Distribution of the channel coefficients and SNR for fading channels

Rayleigh fading: With Rayleigh fading, the coefficients h_{ij} can be modelled as the complex Gaussian variable with the zero mean and variance σ_w^2 in each dimension. The pdf of the coefficient h is then the central chi-square distribution with $2MN$ degrees of freedom

$$f_{\text{Rayleigh}}(h) = \frac{R^{MN}}{(2\sigma_w^2)^{MN} \Gamma(MN)} h^{MN-1} \exp\left\{-\frac{hR}{2\sigma_w^2}\right\}, h \geq 0. \quad (13)$$

Consequently, the instantaneous SNR per symbol γ_s is also chi-square distributed. Using a change of variables, the pdf of γ_s is given by

$$f_{\text{Rayleigh}}(h) = \frac{R^{MN}}{\bar{\gamma}_{ch}^{MN} \Gamma(MN)} \gamma_s^{MN-1} \exp\left\{-\frac{\gamma_s}{\bar{\gamma}_{ch}}\right\}, \gamma_s \geq 0 \quad (14)$$

where $\bar{\gamma}_{ch}$ is the average SNR per channel, which is assumed to be identical for all channels, i.e.

$$\bar{\gamma}_{ch} = \frac{E_s}{NR\mathcal{N}_0} E[\|h_{ij}\|^2] = \frac{2\sigma_w^2 E_s}{NR\mathcal{N}_0}, \quad (15)$$

where $E[\cdot]$ is the mathematical expectation. It can easily be shown that the instantaneous SNR per bit γ_b has the same pdf except that

$$\bar{\gamma}_{ch} = \frac{E_s}{NR\mathcal{N}_0 \log_2 \mathcal{M}} \quad (16)$$

for the \mathcal{M} -ary signal constellation.

Rician fading: For Rician fading, the coefficients h_{ij} can be modelled as a complex Gaussian variable

with the means μ_I and μ_Q for the real and imaginary parts, respectively, and the variance σ_w^2 in each dimension. In this case, $\|\mathbf{H}\|_F^2$ has a non-central chi-square distribution with $2MN$ degrees of freedom. The pdf of h is given by

$$f_{\text{Rician}}(h) = \frac{R}{2\sigma_w^2} \left[\frac{Rh}{s^2} \right]^{\frac{MN-1}{2}} \exp\left\{-\frac{s^2 + Rh}{2\sigma_w^2}\right\} I_{MN-1}\left(\frac{\sqrt{Rh}s}{\sigma_w^2}\right), \quad h \geq 0 \quad (17)$$

where

$$s^2 = MN(\mu_I^2 + \mu_Q^2) \quad (18)$$

is the non-centrality parameter, $I_\alpha(x)$ is the α -th order modified Bessel function of the first kind, which may be represented by the infinite series

$$I_m(x) = \sum_{k=0}^{\infty} \frac{(0.5x)^{n+2k}}{k! \Gamma(n+k+1)}. \quad (19)$$

Introducing the Rician parameter

$$\beta = \frac{\mu_I^2 + \mu_Q^2}{2\sigma_w^2}, \quad (20)$$

the pdf in (13) can be written in the following form

$$f_{\text{Rician}}(h) = \sum_{i=0}^{\infty} \frac{(MN\beta)^i \exp\{-MN\beta\} R^{MN+i}}{\Gamma(i+1)\Gamma(MN+i)(2\sigma_w^2)^{MN+i}} \times h^{MN+i-1} \exp\{-Rh/2\sigma_w^2\}, \quad h \geq 0. \quad (21)$$

Using a change of variables, the pdf of the instantaneous SNR takes the following form:

$$f_{\text{Rician}}(h) = \sum_{i=0}^{\infty} \frac{(MN\beta)^i \exp\{-MN\beta\} \gamma_s^{MN+i-1} \exp\{-\gamma_s/\bar{\gamma}_c\}}{\Gamma(i+1)\Gamma(MN+i)\bar{\gamma}_c^{MN+i}}, \quad \gamma_s \geq 0, \quad (22)$$

where $\bar{\gamma}_c$ is the average SNR per channel, which is assumed to be identical for all channels, as given in (15).

Nakagami- m fading: For Nakagami- m fading with the integer m , $\|h_{ij}\|$ is the amplitude of the channel coefficient h_{ij} and has a Nakagami- m distribution with the variance σ_N^2 in each dimension. The random variable

$$y = R^{-1} \|h_{ij}\|^2 \quad (23)$$

then has the pdf

$$f(y) = \frac{R^m}{(2\sigma^2)^m \Gamma(m)} y^{m-1} \exp\{-Ry/2\sigma^2\}, \quad (24)$$

where $\sigma^2 = \sigma_N^2/m$. Observing that the pdf for Nakagami- m fading has the same form as the pdf for the Rayleigh fading but with $2m$ degree in (13), a single Nakagami- m fading channel is equivalent to an m diversity system for the Rayleigh fading channel. It is then straightforward to show that the results for

STBCs over the Nakagami- m fading channels can be obtained by considering the Rayleigh fading channels with the channel diversity order increased from MN to mMN . Consequently, the pdf of the instantaneous SNR per symbol γ_s can be obtained directly from (10) as

$$f_{Nakagami-m}(\gamma_s) = \frac{1}{\bar{\gamma}_c^{mMN} \Gamma(mMN)} \gamma_s^{mMN-1} \exp\{-\gamma_s/\bar{\gamma}_c\}, \quad (25)$$

where $\bar{\gamma}_c$ is the average SNR per channel, which is assumed to be identical for all channels, as in (15).

3 Capacity Analysis of STBC

3.1 Shannon capacity over fading channels

The capacity of a multiple antenna wireless communication system over a fading channel with continuous-valued inputs and continuous-valued outputs is given in [13] in the following form:

$$C = E \left[\log_2 \det \left(\mathbf{I} + \frac{E_s}{N_e \mathcal{N}_0} \mathbf{H} \mathbf{H}^T \right) \right], \quad [(b/s)/\text{Hz}], \quad (26)$$

where $E[\cdot]$ is the mathematical expectation; \mathbf{I} is the identity matrix with M dimension; $\det(\mathbf{x})$ denotes the determinant of the matrix \mathbf{x} , and the superscript T^* denotes the matrix transpose and conjugate. The capacity of the equivalent STBC channel in (7) with the continuous-valued inputs and continuous-valued outputs for complex signals is given in [4] and [5] as

$$\bar{C} = E \left[R \log_2 \det \left(1 + \frac{E_s}{RN_e \mathcal{N}_0} \|\mathbf{H}\|_F^2 \right) \right] = E[R \log_2(1 + \gamma_s)], \quad [(b/s)/\text{Hz}], \quad (27)$$

Given the pdf of γ_s , the capacity of the equivalent STBC channel can be obtained based on

$$\bar{C} = R \int_0^\infty \log_2(1 + \gamma_s) f(\gamma_s) d\gamma_s, \quad [(b/s)/\text{Hz}], \quad (28)$$

3.2 Capacity of M -ary signal constellations over fading channels

Both (26) and (27) were obtained assuming continuous valued inputs. Here, we consider modulation channels with the discrete-valued multilevel phase inputs and continuous-valued outputs. Assuming maximum likelihood (ML) soft decoding with perfect channel state information at the receiver input, it is well known [14]-[16] that the capacity C_{STBC}^* of the STBC channel (7) can be obtained by averaging the corresponding conditional capacity $\tilde{C}^*(\mathbf{H})$ with respect to the joint pdf of the channel matrix \mathbf{H} . By doing so, the following expression for the capacity C_{STBC}^* of the fading channel is obtained

$$C_{STBC}^* = E[\tilde{C}^*(\mathbf{H})] = \int \tilde{C}^*(\mathbf{H}) f(\mathbf{H}) d\mathbf{H}, \quad [(b/s)/\text{Hz}], \quad (29)$$

with

$$\begin{aligned} \tilde{C}^*(\mathbf{H}) = & R \left\{ \log_2 q - \frac{1}{q\pi R^{-1} \|\mathbf{H}\|_F^2 \mathcal{N}_0} \right. \\ & \times \sum_{j=1}^q \int_{y \in C} \exp \left\{ -\frac{\|y - R^{-1} \|\mathbf{H}\|_F^2 \alpha_j\|^2}{R^{-1} \|\mathbf{H}\|_F^2 \mathcal{N}_0} \right\} \\ & \times \log_2 \left[\sum_{s=1}^q \exp \left\{ \frac{\|y - R^{-1} \|\mathbf{H}\|_F^2 \alpha_j\|^2}{R^{-1} \|\mathbf{H}\|_F^2 \mathcal{N}_0} \right\} \right. \\ & \left. \left. - \frac{\|y - R^{-1} \|\mathbf{H}\|_F^2 \alpha_s\|^2}{R^{-1} \|\mathbf{H}\|_F^2 \mathcal{N}_0} \right\} dy \right\}, \quad (30) \end{aligned}$$

where $\alpha_j, j=1, \dots, q$ is a real signal in the q -ary PAM constellation or complex in the q -ary PSK/QAM constellation, and $f(\mathbf{H})$ is the joint pdf of the $M \times N$ random elements of the channel matrix \mathbf{H} for the fading channel.

Applying the channel model (11), (29) can be simplified to the one-dimensional integral containing the pdf of h

$$C_{STBC,R}^* = E[\tilde{C}^*(h)] = \int \tilde{C}^*(h) f(h) dh, \quad [(b/s)/\text{Hz}], \quad (31)$$

where

$$\begin{aligned} \tilde{C}^*(h) = & R \left\{ \log_2 q - \frac{1}{q\pi h_e \mathcal{N}_0} \sum_{j=1}^q \int_{y \in C} \exp \left\{ -\frac{\|y - h\alpha_j\|^2}{h_e \mathcal{N}_0} \right\} \right. \\ & \times \log_2 \left[\sum_{s=1}^q \exp \left\{ \frac{\|y - h\alpha_j\|^2 - \|y - h\alpha_s\|^2}{h_e \mathcal{N}_0} \right\} \right] dy \right\}. \quad (32) \end{aligned}$$

Note that (31) applies to both the real signal constellations such as PAM, and the complex signal constellations such as the PSK and QAM.

3.3 Capacity comparison

It is shown in [4] that the difference between (26) and (27) is the capacity loss incurred by using a STBC in the multiple-input multiple output (MIMO) wireless communication system over fading channel with the continued valued inputs. The capacity of MIMO fading channel with the PAM, PSK, QAM is given in [15] as

$$C_{M,N}^* = \int \tilde{C}_{M,N}^*(\mathbf{H}) f(\mathbf{H}) d\mathbf{H}, \quad [(b/s)/\text{Hz}], \quad (33)$$

where

$$\begin{aligned} \tilde{C}_{M,N}^*(\mathbf{H}) = & N \log_2 q - q^{-N} (\pi_e \mathcal{N}_0)^{-M} \\ & \times \sum_{\mathbf{x} \in (A_x)^N} \int_{y \in C} \exp \left\{ -\frac{\|\mathbf{y} - \mathbf{H}\mathbf{x}\|^2}{\mathcal{N}_0} \right\} \\ & \times \log_2 \left[\sum_{\mathbf{x}' \in (A_x)^N} \exp \left\{ -\frac{\|\mathbf{y} - \mathbf{H}\mathbf{x}\|^2 - \|\mathbf{y} - \mathbf{H}\mathbf{x}'\|^2}{\mathcal{N}_0} \right\} \right] dy. \quad (34) \end{aligned}$$

Here, N and M are the number of transmit and receive antennas, respectively;

$$Ax \equiv \{\alpha_1, \dots, \alpha_q\} \quad (35)$$

is the q -ary complex signal constellation; $(Ax)^N$ is the N -fold Cartesian product of Ax with itself; the coded vector

$$\mathbf{x} \equiv [x_1, \dots, x_N] \in (Ax)^N \quad (36)$$

is the q^N -variate random variable with outcomes taking values from the expanded signal constellation $(Ax)^N$; and

$$\mathbf{y} \equiv [y_1, \dots, y_M]^T \quad (37)$$

is the M -dimensional output vector of the receive antennas. It can easily be shown that the second terms in (32) and (34) vanish as the SNR increases. This fact implies the capacity of a MIMO fading channel approaches $N \log_2 q$ bit/channel use while the capacity with STBC approaches only $R \log_2 q$ bit/channel use for the large SNR . While the capacity loss of $(N-R) \times \log_2 q$ bit/channel incurred by using STBC is fairly significant, it will be shown below that the SNR threshold for reliable data transmission is reduced because of the STBC diversity gain.

4 Analysis of Error Probability over Fading Channels

4.1 Error probability with Rayleigh fading

Let $P_q^{error}(\gamma_s)$ is the error probability of q -ary signal constellation with STBC in AWGN channel. The error probability with the Rayleigh fading can be obtained by averaging $P_q^{error}(\gamma_s)$ over the pdf of γ_s

$$P_{STBC,q}^{error}(\gamma_s) = \int_0^\infty P_q^{error}(\gamma_s) f_{Rayleigh}(\gamma_s) d\gamma_s \quad (38)$$

Note, $P_q^{error}(\gamma_s)$ can be *SEP* or *BEP*, respectively.

Error probability for PAM: Since full-rate STBCs exist for any number of transmitting antennas using the real PAM constellation [2], $R=1$ for q -ary PAM. The average *SEP* for PAM over AWGN channel is [7]

$$P_q^{error}(\gamma_s) = 2(1-q^{-1})Q\left[\sqrt{6(q^2-1)^{-1}\gamma_s}\right], \quad (39)$$

where $Q(\cdot)$ is the Gaussian tail function. Substituting (14) and (39) into (38), the average *SEP* for PAM is

$$P_{STBC,PAM,q}^{error}(\gamma_s) = \int_0^\infty 2(1-q^{-1})Q\left[\sqrt{6(q^2-1)^{-1}\gamma_s}\right] \times \frac{\gamma_s^{MN-1}}{\bar{\gamma}_c^{MN}\Gamma(MN)} \exp\{-\gamma_s/\bar{\gamma}_c\} d\gamma_s \quad (40)$$

To evaluate the integral in (40), the following integral function can be employed:

$$g(L) = \int_0^\infty Q(\sqrt{ax})x^{L-1} \exp\{-x/u\} dx = 0.5u^L \Gamma(L) \left[1 - \sum_{k=0}^{L-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right], \quad (41)$$

where

$$\mu = \sqrt{\frac{au}{2+au}} \quad (42)$$

The proof is given in Appendix 1. The closed form of the *SEP* for PAM is then given by

$$P_{STBC,PAM,q}^{error}(\gamma_s) = (1-q^{-1}) \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right], \quad (43)$$

where

$$\mu = \sqrt{\frac{3\bar{\gamma}_c}{q^2-1+3\bar{\gamma}_c}} \quad (44)$$

Error probability for PSK: Based on the equivalent scalar AWGN channel model presented before, the error probability for q -ary PSK is equivalent to the analysis in [7] and [17] for adaptive reception of multiphase signals in Rayleigh fading but with MN branch diversity. This approach was also employed in [6]. Following the same steps as in [17], the *SEP* is given by

$$P_{STBC,q}^{error} = \frac{(-1)^{MN-1}(1-\mu^2)^{MN}}{\pi \Gamma(MN)} \left\{ \frac{\partial^{MN-1}}{\partial s^{MN-1}} \left[\frac{1}{s-\mu^2} \left(\frac{\pi}{M} \times (M-1) - \frac{\mu \sin(\pi/M)}{\sqrt{s-\mu^2 \cos^2(\pi/M)}} \right) \right] \right\}_{s=1} \times \cot^{-1} \left(- \frac{\mu \cos(\pi/M)}{\sqrt{s-\mu^2 \cos^2(\pi/M)}} \right) \Bigg|_{s=1}, \quad (45)$$

where

$$\mu = \sqrt{\frac{\bar{\gamma}_c}{1+\bar{\gamma}_c}} \quad (46)$$

and the notation

$$\frac{\partial^{MN-1}}{\partial s^{MN-1}} f(s, \mu) \Bigg|_{s=1}$$

denotes the $(MN-1)$ -th partial derivative of the function $f(s, \mu)$ evaluated at $s=1$. Note that the coherent detection with perfect channel state information at the receiver input is assumed in (45). Following approach in [7], [17], performing the differentiation indicated in (45) and evaluating the resulting function at $s=1$ for $q=2$ and 4, we obtain the following

closed form *BEPs* for the binary phase shift keying (BPSK) and QPSK

$$P_{STBC,2}^{error} = 0.5 \left[1 - \mu \sum_{k=0}^{MN-1} \binom{2k}{k} \left(\frac{1-\mu^2}{4} \right)^k \right], \quad (47)$$

$$P_{STBC,4}^{error} = 0.5 \left[1 - \frac{\mu}{\sqrt{2-\mu^2}} \sum_{k=0}^{MN-1} \binom{2k}{k} \left(\frac{1+\mu^2}{4-2\mu^2} \right)^k \right], \quad (48)$$

respectively. Note that the Gray coding was assumed in the *BEP* calculation for QPSK. The same procedure can be applied to calculate the *SEP* for *q*-ary PSK at $q = 8, 16, 32$, however, the expressions are not as simple as in (47) and (48). In the remainder of this section we employ (38) in order to derive a simpler expression for the error probability.

It is well known [7] that the *BEP* for BPSK and QPSK over the additive white Gaussian noise channel are given as

$$P_{BPSK}^{error}(\gamma_s) = Q(\sqrt{2\gamma_s}), \quad (49)$$

$$P_{QPSK}^{error}(\gamma_s) = Q(\sqrt{\gamma_s}), \quad (50)$$

respectively. As shown in [18], the exact *SEP* of *M*-ary PSK for the AWGN channel can be presented in the following form

$$P_{PSK,AWGN,M}^{error}(\gamma_s) = 2Q\left[\sqrt{2\gamma_s} \sin(\pi/q)\right] - \frac{1}{\pi} \int_{\pi/2-\pi/q}^{\pi/2} \exp\left\{-\gamma_s \frac{\sin^2(\pi/q)}{\cos^2\theta} d\theta\right\} \quad (51)$$

For large *SNR* and large values of *q*, the *SEP* of *q*-ary PSK in the AWGN channel can be approximated as

$$P_{PSK,AWGN,q}^{error}(\gamma_s) \approx 2Q\left[\sqrt{2\gamma_s} \sin(\pi/q)\right] \quad (52)$$

and the equivalent *BEP* is given by

$$P_{PSK,AWGN,q}^{error}(\gamma_s) \approx \frac{SEP_q}{\log q}, \quad (53)$$

where the Gray coding is assumed. This approximation is good for large values of *q*, however, for $q = 2$ there is a difference in the factor of 2 with the exact probability given in (47).

By substituting for $P_{PSK,AWGN,q}^{error}(\gamma_s)$ in (52) and using (41), (38) can be written in the following form

$$P_{STBC,PSK,q}^{error}(\gamma_s) \approx \int_0^\infty 2Q\left[\sqrt{2\gamma_s} \sin(\pi/q)\right] \frac{\gamma_s^{MN-1}}{\bar{\gamma}_c^{MN} \Gamma(MN)} \exp\{-\gamma_s/\bar{\gamma}_c\} d\gamma_s = 1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k}, \quad (54)$$

where

$$\mu = \sqrt{\frac{\sin^2(\pi\gamma_c/q)}{1 + \sin^2(\pi\gamma_c/q)}}. \quad (55)$$

Therefore, the *BEP* can be approximated as

$$P_{STBC,PSK,q}^{error}(\gamma_s) \approx \frac{1}{\log q} \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right]. \quad (56)$$

By substituting for $P_{BPSK}^{error}(\gamma_s)$ or $P_{QPSK}^{error}(\gamma_s)$ in (49) and (50) and using (41), the exact *BEP* for BPSK and QPSK can be derived from (38) as

$$P_{STBC,PSK,q}^{error}(\gamma_s) = \frac{1}{2} \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right], \quad (57)$$

where

$$\mu = \sqrt{\frac{\bar{\gamma}_c}{1 + \bar{\gamma}_c}} \quad (58)$$

for BPSK and

$$\mu = \sqrt{\frac{\bar{\gamma}_c}{2 + \bar{\gamma}_c}} \quad (59)$$

for QPSK, respectively. It can easily be shown that (57) is equivalent to (47) and (48). Using (56), approximations for the *BEPs* of BPSK and QPSK can be obtained as

$$P_{STBC,BPSK,2}^{error} \approx 1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \quad (60)$$

with μ given by (58) and

$$P_{STBC,QPSK,4}^{error} \approx \frac{1}{2} \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right] \quad (61)$$

with μ given by (59), respectively. As expected, this approximation is unsuitable for BPSK, but equation (61) brings us the exact *BEP* for QPSK. It is shown later that this approximation is very accurate for $q > 4$ and large *SNR*.

Error probability for QAM: Rectangular QAM signal constellations are frequently employed because they are equivalent to two PAM signals on quadrature carriers. For *q*-ary, $q = 2^k$ (*k* is even), rectangular QAM, the *SEP* is given in [7] as

$$P_q^{error} = 1 - [1 - P_{\sqrt{q}}^{error}(\gamma_s)]^2, \quad (62)$$

where

$$P_{\sqrt{q}}^{error}(\gamma_s) = 2(1 - q^{-0.5})Q\left(\sqrt{\frac{3}{q-1}}\gamma_s\right). \quad (63)$$

By substituting for P_q^{error} in (63), (38) can be written as

$$P_{STBC,PAM,\sqrt{q}}^{error}(\gamma_s) = \int_0^\infty 2(1 - q^{-0.5})Q\left(\sqrt{\frac{3}{q-1}}\gamma_s\right) \times \frac{\gamma_s^{MN-1} \exp\{\gamma_s/\bar{\gamma}_c\}}{\bar{\gamma}_c^{MN} \Gamma(MN)} d\gamma_s. \quad (64)$$

Using (41), the closed-form *SEP* for the rectangular q -ary QAM is then given by

$$P_{STBC,QAM,q}^{error}(\gamma_s) = 1 - [1 - P_{STBC,PAM,\sqrt{q}}^{error}(\gamma_s)]^2, \quad (65)$$

where

$$P_{STBC,PAM,\sqrt{q}}^{error}(\gamma_s) = (1 - q^{-0.5}) \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1 - \mu^2}{4} \right)^k \binom{2k}{k} \right] \quad (66)$$

and

$$\mu = \sqrt{\frac{3\bar{\gamma}_c}{2q - 2 + 3\bar{\gamma}_c}}. \quad (67)$$

4.2 Error probability over Rician fading

Substituting $f_{Rician}(\gamma_s)$ given by (22) in (38) instead of $f_{Rayleigh}(\gamma_s)$ and following the same procedure used previously, the *SEP* over Rician fading channel can be presented in the following form

$$P_{STBC,Rician,q}^{error}(\gamma_s) = \sum_{n=0}^{\infty} \frac{(MN\beta)^n \exp\{-MN\beta\} \lambda}{\Gamma(n+1)} \times \left[1 - \sum_{k=0}^{MN+n-1} \mu \left(\frac{1 - \mu^2}{4} \right)^k \binom{2k}{k} \right] \quad (68)$$

where

$$\mu = \sqrt{\frac{3\bar{\gamma}_c}{q^2 - 1 + 3\bar{\gamma}_c}} \text{ and } \lambda = 1 - q^{-1} \quad (69)$$

for q -ary PAM,

$$\mu = \sqrt{\frac{\sin^2(\pi\gamma_c/q)}{1 + \sin^2(\pi\gamma_c/q)}} \quad (70)$$

with $\lambda = 0.5$ at $q = 2$ and $\lambda = 1$ at $q > 2$ for q -ary PSK, and

$$\mu = \sqrt{\frac{3\bar{\gamma}_c}{2q - 2 + 3\bar{\gamma}_c}} \text{ and } \lambda = 1 - q^{-0.5} \quad (71)$$

for \sqrt{q} -ary PAM in q -ary rectangular QAM. The *SEP* of q -ary rectangular QAM can then be calculated using (65). Note that each term in the second part of (68) is a monotonically decreasing function of i , and is strictly smaller than 1 for all i . The truncation of the first L terms will introduce an error of at most

$$Error = \frac{\lambda\mu(1 - \mu^{2MN+L})}{1 - \sum_{k=0}^L \frac{(MNK)^k \exp\{-MNK\}}{\Gamma(k+1)}} \quad (72)$$

in the probability of error. The proof is given in Appendix II.

4.3 Error probability under Nakagami- m fading

The probability of error over Nakagami- m , m is the integer, can be obtained from the results presented

in Section 4.1 by increasing the diversity order from MN to mMN . The *SEP* for STBC over a Nakagami- m fading channel is then

$$P_{STBC,Nakagamiq}^{error}(\gamma_s) = \lambda \left[1 - \sum_{k=0}^{MN+n-1} \mu \left(\frac{1 - \mu^2}{4} \right)^k \binom{2k}{k} \right], \quad (73)$$

where μ and λ for q -ary PAM, q -ary PAM, and \sqrt{q} -ary PAM in q -ary rectangular QAM are given by (69)-(71), respectively. The *SEP* of q -ary rectangular QAM can be calculated by (65).

5 Extension to STBC DS-CDMA

There is a great interest in the application of STBCs to practical wireless communications systems constructed based on the generalized approach to signal processing in noise and employing the generalized receiver.

5.1 Generalized receiver

The generalized receiver is constructed in accordance with the generalized approach to signal processing in noise [19]-[21]. The generalized approach to signal processing in noise introduces an additional noise source that does not carry any information about the parameters of desired transmitted signal with the purpose to improve the signal processing system performance. This additional noise can be considered as the reference noise without any information about the parameters of the signal to be detected.

The jointly sufficient statistics of the mean and variance of the likelihood function is obtained under the generalized approach to signal processing in noise employment, while the classical and modern signal processing theories can deliver only a sufficient statistics of the mean or variance of the likelihood function. Thus, the generalized approach to signal processing in noise implementation allows us to obtain more information about the parameters of the desired transmitted signal incoming at the generalized receiver input. Owing to this fact, the detectors constructed based on the generalized approach to signal processing in noise technology are able to improve the signal detection performance of signal processing systems in comparison with employment of other conventional detectors.

The generalized receiver (GR) consists of three channels (see Fig.1): the GR correlation detector channel (GR CD) – the preliminary filter (PF), the multipliers 1 and 2, the model signal generator (MSG); the GR energy detector channel (GR ED) – the PF, the additional filter (AF), the multipliers 3 and 4, the summator 1; and the GR compensation channel (GR CC) – the summators 2 and 3, the acc-

umulator 1. The threshold apparatus (THRA) device defines the GR threshold. As we can see from Fig.1, there are two band-pass filters, i.e. the linear systems, at the GR input, namely, the PF and AF. We assume for simplicity that these two filters or linear systems have the same amplitude-frequency characteristics or impulse responses. The AF central frequency is detuned relative to the PF central frequency.

There is a need to note the PF bandwidth is matched with the transmitted signal bandwidth. If the detuning value between the PF and AF central frequencies is more than 4 or 5 times the transmitted signal bandwidth to be detected, i.e. $4 \div 5 \Delta f_s$, where Δf_s is the transmitted signal bandwidth, we can believe that the processes at the PF and AF outputs are uncorrelated because the coefficient of correlation between them is negligible (not more than 0.05). This fact was confirmed experimentally in [22] and [23] independently. Thus, the transmitted signal plus noise can be appeared at the GR PF output and the

noise only is appeared at the GR AF output. The stochastic processes at the GR AF and GR PF outputs present the input stochastic samples from two independent frequency-time regions. If the discrete-time noise $w_i[k]$ at the GR PF and GR AF inputs is Gaussian, the discrete-time noise $\zeta_i[k]$ at the GR PF output is Gaussian too, and the reference discrete-time noise $\eta_i[k]$ at the GR AF output is Gaussian owing to the fact that the GR PF and GR AF are the linear systems and we believe that these linear systems do not change the statistical parameters of the input process. Thus, the GR AF can be considered as a generator of the reference noise with a priori information a “no” transmitted signal (the reference noise sample) [21, Chapter 5]. The noise at the GR PF and GR AF outputs can be presented as

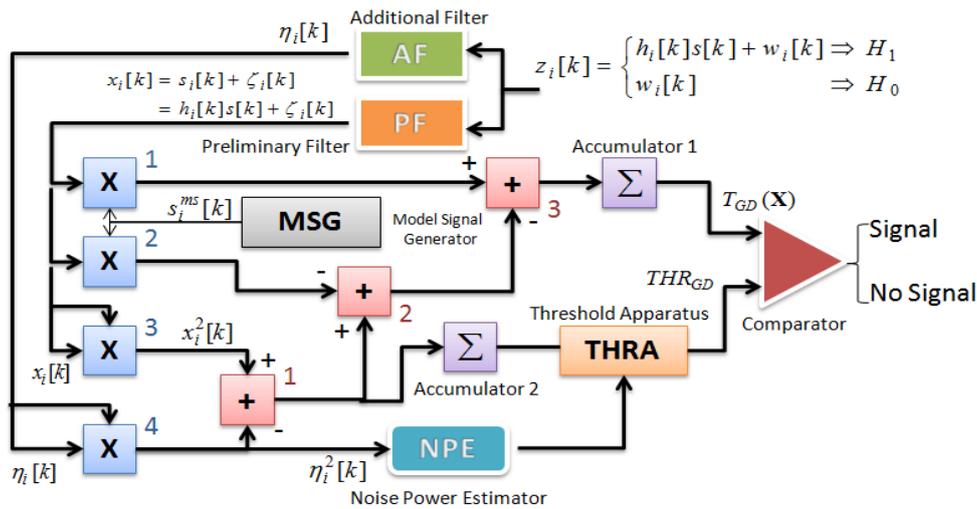


Fig. 1. Generalized receiver structure.

$$\begin{cases} \zeta_i[k] = \sum_{m=-\infty}^{\infty} g_{PF}[m]w_i[k-m] ; \\ \eta_i[k] = \sum_{m=-\infty}^{\infty} g_{AF}[m]w_i[k-m] , \end{cases} \quad (74)$$

where $g_{PF}[m]$ and $g_{AF}[m]$ are the impulse responses of the GR PF and GR AF, respectively.

In a general, under practical implementation of any detector in wireless communication system with sensor array, the bandwidth of the spectrum to be sensed is defined. Thus, the GR AF bandwidth and central frequency can be assigned, too (this bandwidth cannot be used by the transmitted signal because it is out of its spectrum). The case when there

are interfering signals within the GR AF bandwidth, the action of this interference on the GR detection performance, and the case of non-ideal condition when the noise at the GR PF and GR AF outputs is not the same by statistical parameters are discussed in [24] and [25].

Under the hypothesis \mathcal{H}_1 (“a yes” transmitted signal), the GR CD generates the signal component $s_i^m[k]s_i[k]$ caused by interaction between the model signal $s_i^m[k]$, forming at the MSG output, and the incoming signal $s_i[k]$, and the noise component $s_i^m[k] \times \zeta_i[k]$ caused by interaction between the model sig-

nal $s_i^m[k]$ and the noise $\zeta_i[k]$ at the PF output. GR ED generates the transmitted signal energy $s_i^2[k]$ and the random component $s_i[k]\zeta_i[k]$ caused by interaction between the transmitted signal $s_i[k]$ and the noise $\zeta_i[k]$ at the PF output. The main purpose of the GR CC is to cancel completely in the statistical sense the GR CD noise component $s_i^m[k]\zeta_i[k]$ and the GR ED random component $s_i[k]\zeta_i[k]$ based on the same nature of the noise $\zeta_i[k]$. The relation between the transmitted signal to be detected $s_i[k]$ and the model signal $s_i^m[k]$ is defined as:

$$s_i^m[k] = \mu s_i[k], \quad (75)$$

where μ is the coefficient of proportionality.

The main functioning condition under the GR employment in any signal processing system including the communication one with radar sensors is the equality between the parameters of the model signal $s_i^m[k]$ and the incoming signal $s_i[k]$, for example, by amplitude. Under this condition it is possible to cancel completely in the statistical sense the noise component $s_i^m[k]\zeta_i[k]$ of the GR CD and the random component $s_i[k]\zeta_i[k]$ of the GR ED. Satisfying the GR main functioning condition given by (75), $s_i^m[k] = s_i[k]$, $\mu = 1$, we are able to detect the transmitted signal with the high probability of detection at the low SNR and define the transmitted signal parameters with high accuracy.

Practical realization of this condition (75) at $\mu \rightarrow 1$ requires increasing in the complexity of GR structure and, consequently, leads us to increasing in computation cost. For example, there is a need to employ the amplitude tracking system or to use the off-line data samples processing. Under the hypothesis \mathcal{H}_0 ("a no" transmitted signal), satisfying the main GR functioning condition (75) at $\mu \rightarrow 1$ we obtain only the background noise $\eta_i^2[k] - \zeta_i^2[k]$ at the GR output.

Under practical implementation, the real structure of GR depends on specificity of signal processing systems and their applications, for example, the radar sensor systems, adaptive wireless communication systems, cognitive radio systems, satellite communication systems, mobile communication systems and so on. In the present paper, the GR circuitry (Fig.1) is demonstrated with the purpose to explain the main functioning principles. Because of this, the GR flowchart presented in the paper should be considered under this viewpoint. Satisfying the GR main fu-

ctioning condition (75) at $\mu \rightarrow 1$, the ideal case, for the wireless communication systems with radar sensor applications we are able to detect the transmitted signal with very high probability of detection and define accurately its parameters.

In the present paper, we discuss the GR implementation in communication systems using the radar sensor array. Since the presented GR test statistics is defined by the signal energy and noise power, the equality between the parameters of the model signal $s_i^m[k]$ and transmitted signal to be detected $s_i[k]$, in particular by amplitude, is required that leads us to high circuitry complexity in practice. For example, there is a need to employ the amplitude tracking system or off-line data sample processing. Detailed discussion about the main GR functioning principles if there is no a priori information and there is an uncertainty about the parameters of transmitted signal, i. e., the transmitted signal parameters are random, can be found in [19] and [20, Chapter 6, pp.611–621 and Chapter 7, pp. 631–695].

The complete matching between the model signal $s_i^m[k]$ and the incoming signal $s_i[k]$, for example by amplitude, is a very hard problem in practice because the incoming signal $s_i[k]$ depends on both the fading and the transmitted signal parameters and it is impractical to estimate the fading gain at the low SNR. This matching is possible in the ideal case only. The GD detection performance will be deteriorated under mismatching in parameters between the model signal $s_i^m[k]$ and the transmitted signal $s_i[k]$ and the impact of this problem is discussed in [26]–[29], where a complete analysis about the violation of the main GR functioning requirements is presented. The GR decision statistics requires an estimation of the noise variance σ_η^2 using the reference noise $\eta_i[k]$ at the AF output.

Under the hypothesis \mathcal{H}_1 , the signal at the GR PF output, see Fig. 1, can be defined as

$$x_i[k] = s_i[k] + \zeta_i[k], \quad (76)$$

where $\zeta_i[k]$ is the noise at the PF output and

$$s_i[k] = h_i[k]s[k], \quad (77)$$

where $h_i[k]$ are the channel coefficients. Under the hypothesis \mathcal{H}_0 and for all i and k , the process $x_i[k] = \zeta_i[k]$ at the PF output is subjected to the complex Gaussian distribution and can be considered as the i.i.d. process.

In the ideal case, we can think that the signal at the GR AF output is the reference noise $\eta_i[k]$ with the same statistical parameters as the noise $\zeta_i[k]$. In practice, there is a difference between the statistical

parameters of the noise $\eta_i[k]$ and $\zeta_i[k]$. How this difference impacts on the GR detection performance is discussed in detail in [20, Chapter 7, pp. 631-695] and in [26]-[29],

The decision statistics at the GR output presented in [19] and [20, Chapter 3] is extended for the case of antenna array when an adoption of multiple antennas and antenna arrays is effective to mitigate the negative attenuation and fading effects. The GR decision statistics can be presented in the following form:

$$T_{GR}(\mathbf{X}) = \sum_{k=0}^{N-1} \sum_{i=1}^M 2x_i[k]s_i^m[k] - \sum_{k=0}^{N-1} \sum_{i=1}^M x_i^2[k] + \sum_{k=0}^{N-1} \sum_{i=1}^M \eta_i^2[k] - \sum_{k=0}^{N-1} \sum_{i=1}^M \zeta_i^2[k] \stackrel{\mathcal{H}_1}{>} \stackrel{\mathcal{H}_0}{<} THR_{GR}, \quad (78)$$

where

$$\mathbf{X} = [\mathbf{x}(0), \dots, \mathbf{x}(N-1)] \quad (79)$$

is the vector of the random process at the GR PF output and THR_{GR} is the GR detection threshold.

Under the hypotheses \mathcal{H}_1 and \mathcal{H}_0 and when the amplitude of the transmitted signal is equal to the amplitude of the model signal, $s_i^m[k] = s_i[k]$, $\mu = 1$, the GR decision statistics $T_{GD}(\mathbf{X})$ takes the following form in the statistical sense, respectively:

$$\begin{cases} \mathcal{H}_1 : T_{GD}(\mathbf{X}) = \sum_{k=0}^{N-1} \sum_{i=1}^M s_i^2[k] + \sum_{k=0}^{N-1} \sum_{i=1}^M \eta_i^2[k] - \sum_{k=0}^{N-1} \sum_{i=1}^M \zeta_i^2[k], \\ \mathcal{H}_0 : T_{GD}(\mathbf{X}) = \sum_{k=0}^{N-1} \sum_{i=1}^M \eta_i^2[k] - \sum_{k=0}^{N-1} \sum_{i=1}^M \zeta_i^2[k]. \end{cases} \quad (80)$$

In (80) the term $\sum_{k=0}^{N-1} \sum_{i=1}^M s_i^2[k] = E_s$ corresponds to the average transmitted signal energy, and the term $\sum_{k=0}^{N-1} \sum_{i=1}^M \eta_i^2[k] - \sum_{k=0}^{N-1} \sum_{i=1}^M \zeta_i^2[k]$ is the background noise at the GR output. The GR output background noise is a difference between the noise power at the GR PF and GR AF outputs. Practical implementation of the GR decision statistics requires an estimation of the noise variance σ_η^2 using the reference noise $\eta_i[k]$ at the AF output.

5.2 System model

To facilitate the analysis, we generalize the CDMA multiple access interference model from [30] and [31] to accommodate multiple antennas. The system model is presented in Fig.2. In the transmitter, S information symbols for K users are encoded by the respective STBC encoders, and then spread by each user's pseudonoise code, modulated and transmitted

from N transmitting antennas over the symbol duration T , simultaneously. At the receivers, each user has M receive antennas, and the filtered signals are first disspread, and then sent to STBC decoders. The symbol decisions are made based on the M STBC decoder outputs. The signal at the j -th receive input antenna is given by

$$z_j(t) = \sum_{n=1}^N \sum_{k=1}^K \sqrt{2P_k} h_{knj}(t) a_k(t - \tau_{knj}) b_{nk}(t - \tau_{knj}) \times \cos[\omega_c(t - \tau_{knj})] + w(t), \quad (81)$$

where $h_{knj}(t)$ is the channel coefficient from the n -th transmitting antenna to the j -th receive antenna for the k -th user; $P_k = E_s/T_s$ is the symbol power of the k -th user; E_s is the symbol energy; T_s is the symbol duration; $a_k(t)$ is the PN spreading chip sequence with chip duration T_c ; $w(t)$ is the zero mean AWGN with the power spectral density $\sigma_w^2/2$ in each real dimension; τ_{knj} is the time delay from the n -th transmitting antenna to the j -th receive antenna; ω_c is the carrier frequency; $b_{nk}(t)$ is the encoded signal transmitted from the n -th antenna of user k . Binary modulation is assumed in this model.

5.3 Channel model analysis

To facilitate the analysis, we assume the first user is the desired one, without loss of generality. The disspread signal input to the j -th STBC decoder for the i -th received symbol is

$$\begin{aligned} \hat{z}_{1j}(t) &= \sum_{q=1}^N \int_{(i-1)T_s}^{iT_s} \left[\sqrt{2P_k} \sum_{n=1}^N \sum_{k=1}^K h_{knj}(t) a_k(t - \tau_{knj}) \right. \\ &\quad \times b_{nk}(t - \tau_{knj}) \cos[\omega_c(t - \tau_{knj})] + w(t) \left. \right] a_1(t - \tau_{1qj}) \\ &\quad \times \cos[\omega_c(t - \tau_{1qj})] dt \\ &= \sqrt{\frac{P_1}{2}} T_s \sum_{n=1}^N h_{1nj}^{(i)} b_{n1}^{(i)} + \int_{(i-1)T_s}^{iT_s} \left[\sqrt{2P_k} \sum_{n=1}^N \sum_{\substack{q=1 \\ q \neq n}}^N h_{knj}(t) a_1(t - \tau_{1nj}) \right. \\ &\quad \times b_{n1}(t - \tau_{1nj}) \cos[\omega_c(t - \tau_{1nj})] \left. \right] a_1(t - \tau_{1nj}) \cos[\omega_c(t - \tau_{1nj})] dt + \sum_{q=1}^N \int_{(i-1)T_s}^{iT_s} w(t) a_1(t - \tau_{1nj}) \cos[\omega_c(t - \tau_{1nj})] dt. \end{aligned} \quad (82)$$

Note that only the first term of (82) is the desired signal; the second term of (82) is the multiple access interference (MAI) produced by the same user from different transmit antennas; the third term of (82) is the MAI produced by other users; the fourth term of (82) is the AWGN. Using the Gaussian approximation in [30], (82) can be presented in the following form

$$\hat{z}_{1j}(t) = \sqrt{0.5P_1T_s} \sum_{n=1}^N h_{1nj} b_{n1} + \eta_{1j} \quad (83)$$

where $\hat{z}_{1j}(t)$ is the Gaussian random variable; η_{1j} is the combination of the interference and noise. The expected mean and variance of η_{1j} are given by

$$\begin{cases} E[\eta_{1j}] = 0; \\ Var[\eta_{1j}] = N(N-1) \frac{T_s^2}{6G} \sum_{k=1}^K P_k + 4\sigma_w^4 NT_s \end{cases}, \quad (84)$$

respectively, where G is the processing gain of the DS-CDMA system. Note that (83) has the same

form as (4). After STBC decoding is performed on $\hat{z}_{1j}(t)$ given in (83), the decision statistic for user 1 over T symbol durations takes the form

$$\hat{z}_1(t) = R^{-1} \sqrt{0.5P_1T_s} \|\mathbf{H}\|_F^2 \mathbf{b}_{1T} + \boldsymbol{\eta}_T, \quad (85)$$

where $\eta_{iT}(t)$ has the zero mean and the variance is defined as

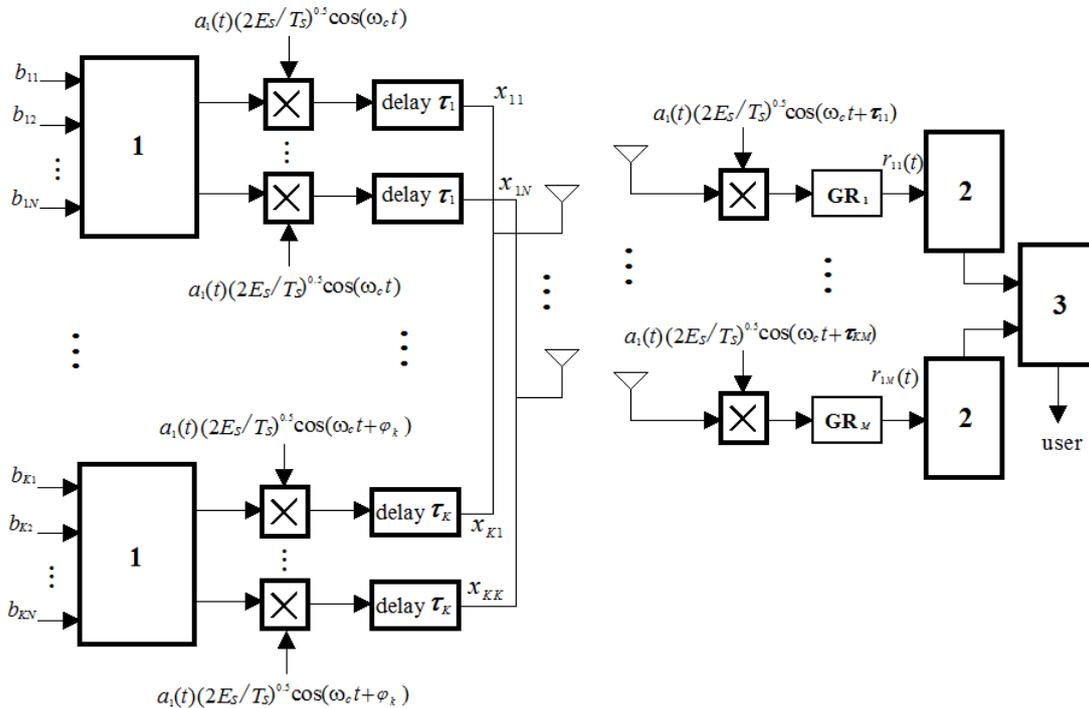


Fig. 2. System model for STBC DS-CDMA with multiple antennas employing the generalized receiver: 1 – STBC Encoder; 2 – STBC Decoder; 3 – Decision device; GR - Generalized receiver.

$$Var\{\eta_{iT}(t)\} = \frac{1}{R} \|\mathbf{H}\|_F^2 \left[\frac{N(N-1)T_s^2}{6G} \sum_{k=1}^K P_k + NT_s 4\sigma_w^4 \right]. \quad (86)$$

Therefore, the effective instantaneous SNR at the generalized receiver output is given by

$$\gamma_s = \left\{ \frac{N(N-1)K}{3G} + \frac{4N\sigma_w^4}{E_s^2} \right\}^{-1} R^{-1} \|\mathbf{H}\|_F^2. \quad (87)$$

Note that the perfect power control is assumed in (87), i.e., $P_k = P_1$.

5.4 Capacity analysis of STBC-CDMA

To facilitate the capacity analysis, we first normalize the equivalent channel by $\sqrt{0.5T_s}$, then (85) can be written in the same form as (7)

$$\mathbf{y}_{nT} = R^{-1} \|\mathbf{H}\|_F^2 \mathbf{x}_{nT} + \boldsymbol{\eta}_{nT}, \quad (88)$$

where \mathbf{x}_{nT} is the $S \times 1$ complex input matrix with each entry having symbol energy E_s ; the combination of the interference and noise $\boldsymbol{\eta}_{nT}$ has the zero mean and variance

$$Var\{\boldsymbol{\eta}_{nT}\} = R^{-1} \frac{\|\mathbf{H}\|_F^2 N(N-1)K}{3G} + 4\sigma_w^4 N. \quad (89)$$

The capacity of this STBC CDMA system constructed based on the generalized approach to signal processing in noise [19]-[21] and employing a q -ary signal constellation can be obtained directly from (31).

5.5 Probability of error for DS-CDMA with STBC

The average SNR per channel is determined as

$$\begin{aligned} \bar{\gamma}_c &= \frac{E\{|h_{ij}|^2\}}{R\left\{\frac{N(N-1)K}{3G} + \frac{4N\sigma_w^4}{E_s^2}\right\}} \\ &= \frac{2\sigma^2}{R\left\{\frac{N(N-1)K}{3G} + \frac{4N\sigma_w^4}{E_s^2}\right\}} \end{aligned} \quad (90)$$

and this can be used with the probability of error results in Section 4 to obtain the performance in fading channels. In particular, the exact BEP of BPSK is given by

$$P_{STBC_CDMA,Rayleigh,2b}^{error} = \frac{1}{2} \left[1 - \sum_{k=0}^{MN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right] \quad (91)$$

for the Rayleigh fading channel;

$$\begin{aligned} P_{STBC_CDMA,Rician,2b}^{error} &= \sum_{n=0}^{\infty} \frac{(MN\beta)^n \exp\{-MN\beta\}}{2\Gamma(n+1)} \lambda \\ &\times \left[1 - \sum_{i=0}^{MN+n-1} \mu \left(\frac{1-\mu^2}{4} \right)^i \binom{2i}{i} \right] \end{aligned} \quad (92)$$

for the Rician fading channel;

$$P_{STBC_CDMA,Naragamiq}^{error} = \frac{\lambda}{2} \left[1 - \sum_{k=0}^{mMN-1} \mu \left(\frac{1-\mu^2}{4} \right)^k \binom{2k}{k} \right] \quad (93)$$

for the Nakagami- m fading channel, where μ is given by (58) and $\bar{\gamma}_c$ is defined in (90). Note that there are two factors in $\bar{\gamma}_c$ which determine the BEP of the DS-CDMA wireless communication system with STBC, $N(N-1)K/3G$ and $4\sigma_w^4 N$. The first term corresponds to the MAI from other users and the self-interference from different transmitting antennas. The second term corresponds to the system noise, i.e., AWGN. At the high SNR, $\bar{\gamma}_c$ will be dominated on the MAI, i.e., the number of users limits the performance, as expected.

6 Numerical results

In this section, some numerical results are presented to illustrate and verify the capacity and probability of error results obtained before. Figure 3 demonstrates the capacity using SBTC G_2 over Rician fading channel with one, two and four receive antennas for BPSK, QPSK, and 8-PSK. The Rician parameter is $\beta=100$. This figure shows that the capacity with STBC G_2 is not increased as the number of receiving

antennas increases. However, the SNR threshold required to achieve capacity improves as the number of receive antennas increased. The capacity with a single antenna over Rician fading channel for PSK is included for reference. Additionally, Fig. 3 represents a superiority of employment of the generalized receiver in DS-CDMA wireless communication system in comparison with the correlation one.

The capacity using several STBCs over Rayleigh fading channel is presented in Fig.4. As expected, it shows that G_2 is the optimal code from a capacity perspective, and H_4 is more efficient in comparison with G_4 . Also, a demonstration of superiority to employ the generalized receiver in comparison with the correlation one in DS-CDMA wireless communication system with STBCs is demonstrated in Fig.4. Comparison between Figs. 3 and 4 demonstrates that the DS-CDMA wireless communication system with STBC codes achieves the capacity at the lower

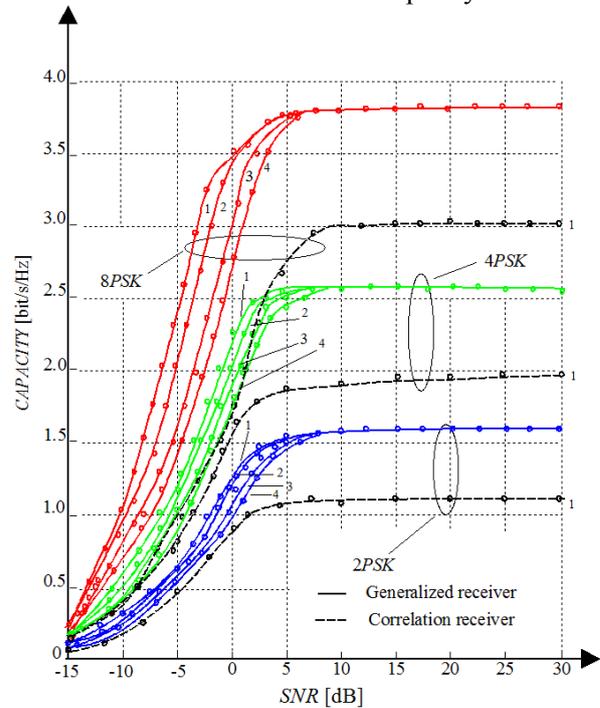


Fig. 3. Capacity of DS-CDMA system employing STBC G_2 over Rician fading channel with Rician parameter $\beta=100$: 1 – MIMO 4x2; 2 – MIMO 2x2; 3 – MIMO 1x2; 4 – MIMO 1x1.

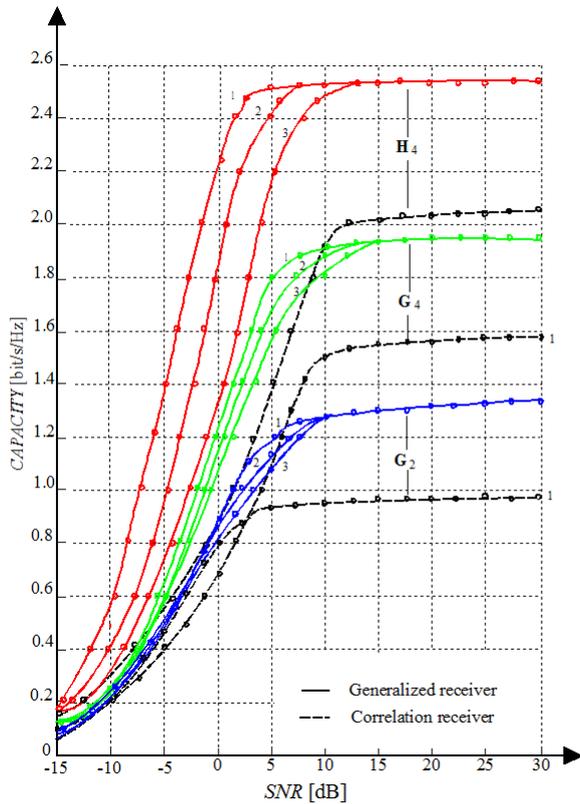


Fig. 4. Capacity of DS-CDMA system employing various STBCs over Rayleigh fading channel: 1 – MIMO 4x2; 2 – MIMO 2x2; 3 – MIMO 1x2.

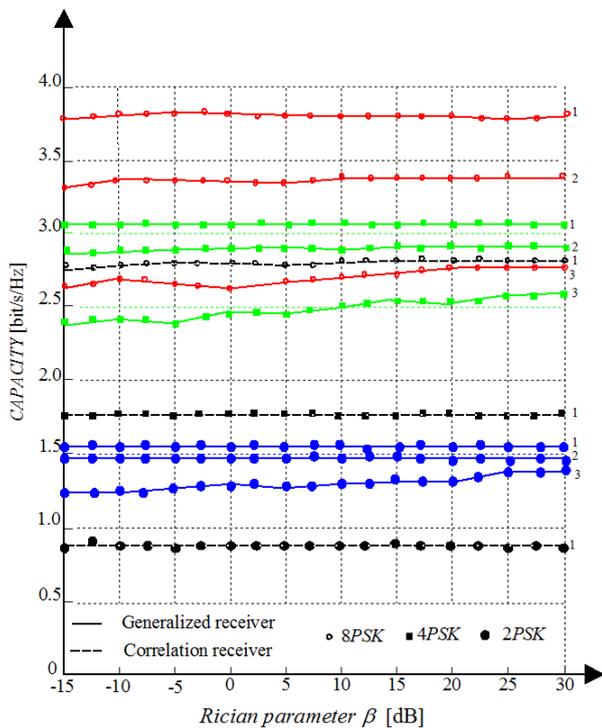


Fig. 5. Capacity of DS-CDMA system with STBC G_2 versus the Rician parameter β ; $SNR = 5$ dB: 1 – MIMO 4x2; 2 – MIMO 2x2; 3 – MIMO 1x2.

SNR over the Rician fading channel at $\beta = 100$ than

the Rayleigh fading channel. Figure 5 demonstrates the relationship between the Rician parameter β and the capacity if STBC code G_2 is used. Note that the capacity is insensitive to the Rician parameter when $\beta > 15$ dB. Additionally, we can see a superiority of implementation of the generalized receiver over the correlation one in DS-CDMA wireless communication system with STBC codes.

Simulation was used to verify the exact and approximate error probabilities given in Section 4. In Fig.6, the BEP of QPSK at STBCs G_2 , G_3 , G_4 , H_3 and H_4 with one and two receive antennas are presented, and these results are identical to those obtained using (48). Also, a superiority of employment of the generalized receiver in DS-CDMA system with STBC in comparison with the correlation one is evident. Figure 7 shows the comparison between the approximate and exact (via simulation) SEP for the 8-PSK. Note that the approximation error is negligible. Figure 8 demonstrates the SEP for the 16-QAM with one and two receive antennas for different STBCs. A superiority of implementation of the generalized receiver in DS-CDMA system with STBC over the correlation one is presented, too. These results are identical to those obtained with (39).

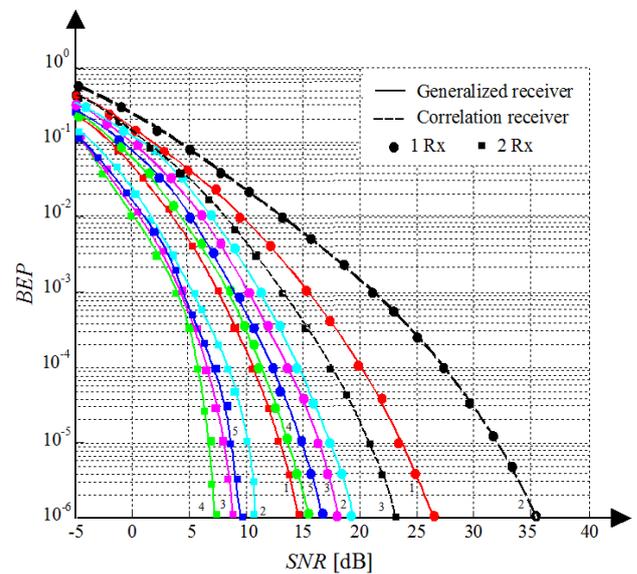


Fig. 6. BEP of DS-CDMA system with QPSK for STBC using one and two receive antennas over Rayleigh fading channel: 1 – STBC G_2 ; 2 – STBC G_3 ; 3 – STBC H_3 ; 4 – STBC G_4 ; 5 – STBC H_4 .

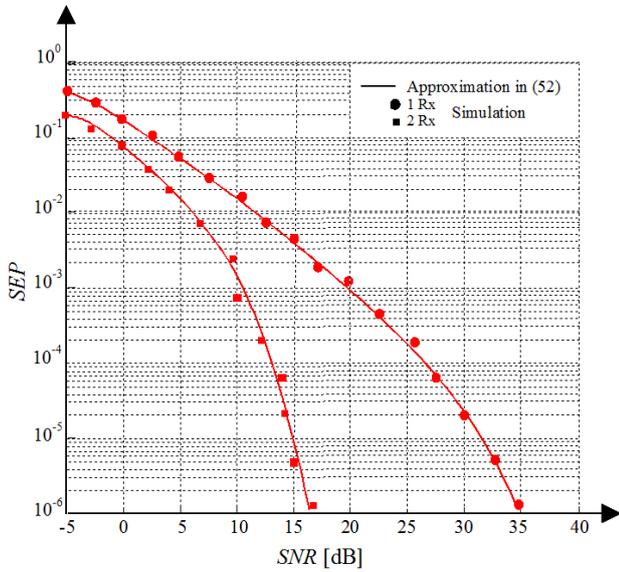


Fig. 7. *SEP* of DS-CDMA system with QPSK for STBC using one and two receive antennas over Rayleigh fading channel: 1 – STBC \mathbf{G}_2 ; 2 – STBC \mathbf{G}_3 ; 3 – STBC \mathbf{H}_3 ; 4 – STBC \mathbf{G}_4 ; 5 – STBC \mathbf{H}_4 .

In Fig.9 the capacity of DS-CDMA wireless communication system based on the generalized approach to signal processing in noise [19]-[21] with several STBCs is demonstrated for the case of BPSK modulation over the Rayleigh fading channel. We can see that with a given number of users and signal processing gain, the system may not be able to achieve the full channel capacity even with infinite

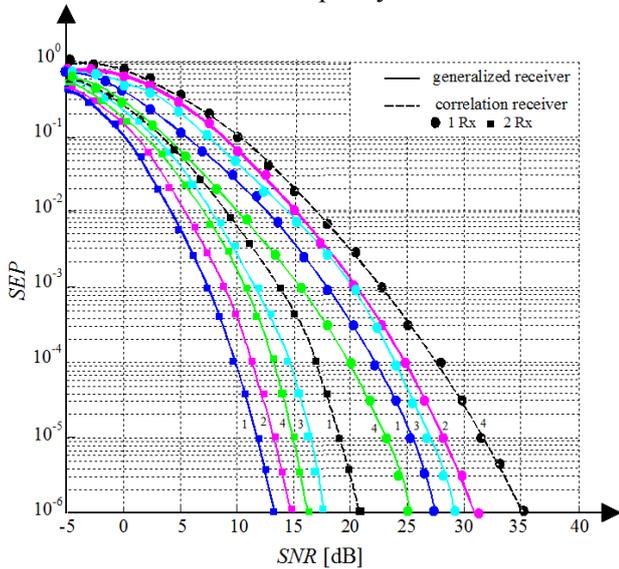


Fig. 8. *SEP* of DS-CDMA system with 16-QAM for STBC using one and two receive antennas over Rayleigh fading channel: 1 – STBC \mathbf{H}_4 ; 2 – STBC \mathbf{H}_3 ; 3 – STBC \mathbf{G}_3 ; 4 – STBC \mathbf{G}_4 .

SNR due to the dominant MAI component. In this case, increasing the number of antennas will incre-

ase the achievable DS-CDMA wireless communication system capacity. Note that the DS-CDMA wireless communication system capacity increases significantly as the number of receive antennas increases for a given number of users and signal processing gain, as expected. However, it should be noted that if the DS-CDMA wireless communication system can already achieve the channel capacity for a given number of antennas, users and signal processing gain, increasing the number of antennas cannot increase the DS-CDMA wireless communication system capacity.

Figure 10 presents us the relationship between the DS-CDMA wireless communication system capacity and the number of users given the processing gain and SNR over the Rayleigh fading channel. It can be seen that the capacity decreases rapidly as the number of users is increased for one and two receive antennas. However, with four receive antennas increasing the number of users has much less effect on the DS-CDMA wireless communication capacity.

The *BEP* for DS-CDMA wireless communication system constructed on the basis of the generalized approach to signal processing in noise with STBC using BPSK modulated signals is presented in Fig. 11 for one, two, three, and four receive antennas. The signal processing gain is 64, the number of users is 20 and the Rayleigh fading is employed for all DS-CDMA wireless communication system figures. Figure 11 presents that significant performance gain

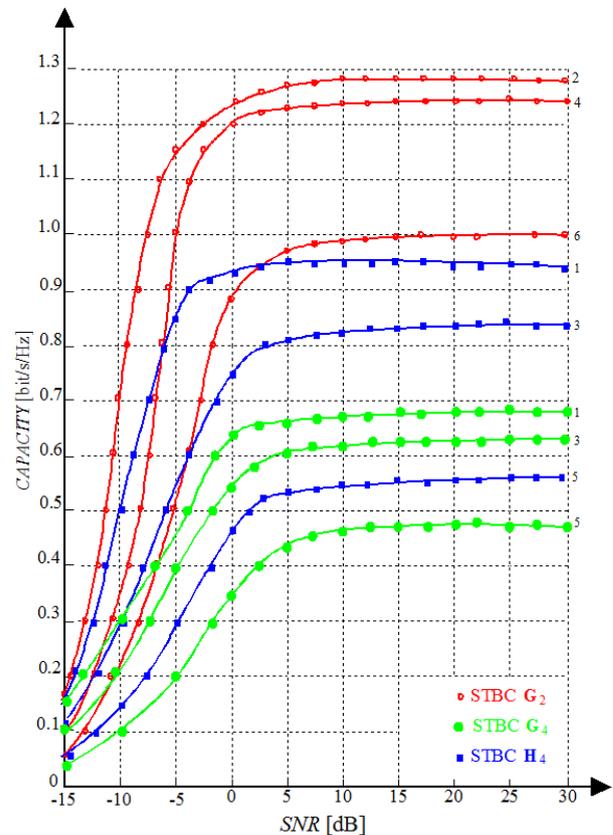


Fig. 9. Capacity of DS-CDMA system with BPSK, STBC over Rayleigh fading channel $G = 32, K = 30:1$ – MIMO 4x4; 2 – MIMO 4x2; 3 – MIMO 2x4; 4 – MIMO 2x2; 5 – MIMO 1x4; 6 – MIMO 1x2.

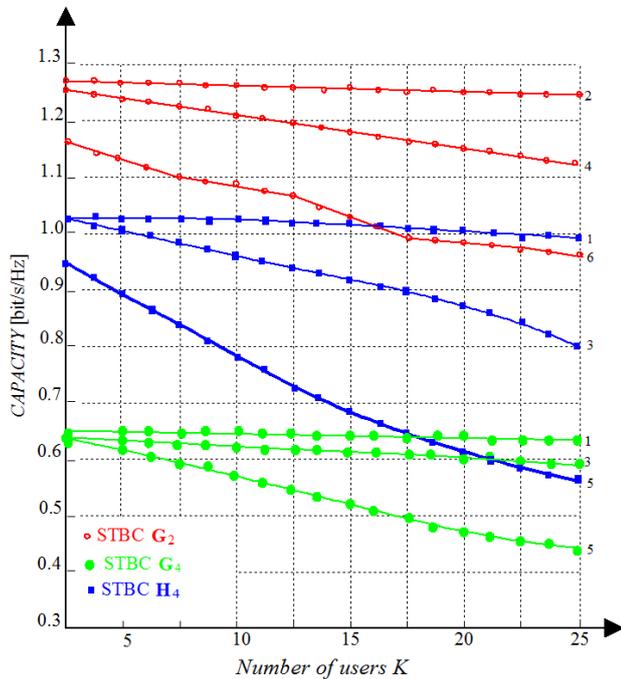


Fig. 10. Capacity of DS-CDMA system with BPSK and STBC over Rayleigh fading channel $G = 32, SNR = 7$ dB: 1 – MIMO 4x4; 2 – MIMO 4x2; 3 – MIMO 2x4; 4 – MIMO 2x2; 5 – MIMO 1x4; 6 – MIMO 1x2.

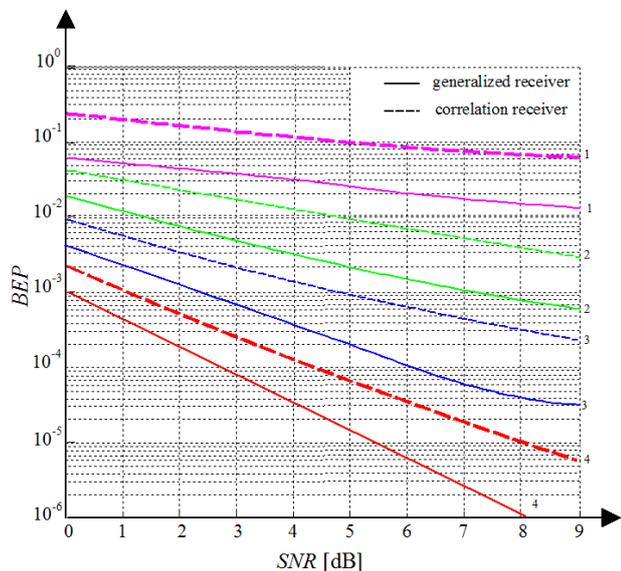


Fig. 11. BEP of DS-CDMA system with BPSK and STBC G_2 over Rayleigh fading channel $G = 64, K = 20$: 1 – one receive antenna; 2 – two receive antennas; 3 – three receive antennas; 4 – four receive antennas.

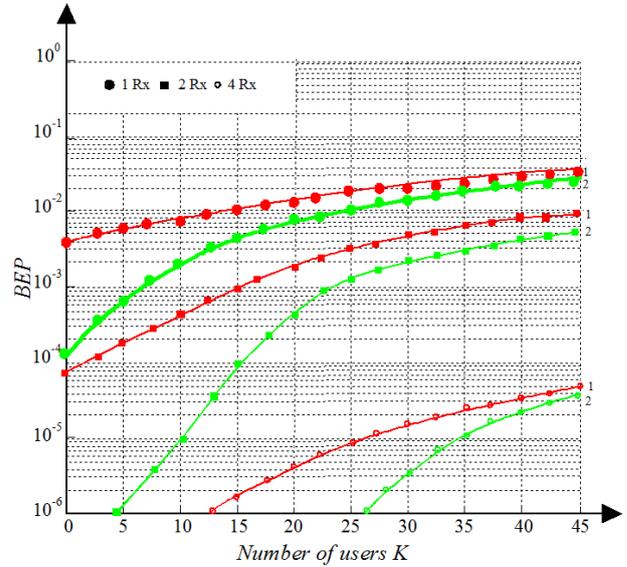


Fig. 12. BEP versus the number of users for DS-CDMA system with BPSK, STBC G_2 (the curve 1) and G_4 (the curve 2) over the Rayleigh fading channel with $G = 64, SNR = 7$ dB.

can be obtained with multiple receive antennas. For comparison the simulation results for the correlation receiver are presented, too. We can see a great superiority of implementation of the generalized receiver in DS-CDMA wireless communication system with STBC over the correlation one.

Figure 12 demonstrates the relationship between the BEP and the number of users in the DS-CDMA wireless communication system at SNR equal to 7 dB with G_2 and G_4 . As the number of users is increased, the performance degrades, but at the four receive antennas the DS-CDMA wireless communication system is capable of accommodating far more users than with one receive antenna. As it is shown in the Fig. 12, G_4 provides the better performance than G_2 , however, this is obtained at the price of the capacity loss as shown in Fig. 10.

7 Conclusions

The capacity and error probability of STBCs employed by DS-CDMA wireless communication system with STBC constructed on the basis of the generalized approach to signal processing in noise have been studied in fading channels for q -ary signal constellations. The Rayleigh, Rician, and Nakagami- m fading channels were investigated for the PAM, PSK, and QAM modulations. The closed form of the error probabilities under employment of the generalized receiver based on the generalized approach to signal processing in noise were derived for various fading

and modulation combinations. This analysis has been employed to determine the performance of STBC multiuser DS-CDMA wireless communication system. Comparative analysis concerning implementation of the generalized receiver and correlation one in DS-CDMA wireless communication system with STBCs demonstrates a great superiority in favor of the first.

Appendix 1

Using integration by parts, the proof of (41) is as follows:

$$\begin{aligned}
 g(L) &= \int_0^{\infty} Q(\sqrt{ax})x^{L-1} \exp\{-x/u\} dx \\
 &= -\int_0^{\infty} Q(\sqrt{ax})x^{L-1} u d\{\exp[-x/u]\} \\
 &= -Q(\sqrt{ax})x^{L-1} u \exp\{-x/u\} \\
 &\quad + \int_0^{\infty} \exp\{-x/u\} u [Q(\sqrt{ax})x^{L-1}] dx \\
 &= u(L-1) \int_0^{\infty} \exp\{-x/u\} Q(\sqrt{ax})x^{L-2} dx \\
 &\quad - u\sqrt{a/8\pi} \int_0^{\infty} x^{L-3/2} \exp\{-x/u\} \exp\{-ax/2\} dx \\
 &= u(L-1)g(L-1) - \frac{1}{2}u^L \mu \left(\frac{1-\mu^2}{4}\right)^{L-1} \frac{(2L-2)!}{(L-1)!}, \quad (87)
 \end{aligned}$$

where

$$\mu = \sqrt{\frac{au}{2+au}}. \quad (95)$$

Repeating the process, we have

$$g(L) = u^{L-1}\Gamma(L)g(1) - \frac{1}{2}u^L\Gamma(L)\sum_{k=2}^L \mu \left(\frac{1-\mu^2}{4}\right)^{k-1} \binom{2k-2}{k-1} \quad (96)$$

Now, using the fact that

$$g(1) = \int_0^{\infty} Q(\sqrt{ax}) \exp\{-x/u\} dx = \frac{1}{2}u(1-\mu), \quad (97)$$

we obtain (41)

$$g(L) = \frac{1}{2}u^L\Gamma(L) \left[1 - \sum_{k=0}^{L-1} \mu \left(\frac{1-\mu^2}{4}\right)^k \binom{2k}{k} \right]. \quad (98)$$

Appendix 2

The truncation of (68) to the first L terms will introduce the error

$$Error = \lambda \sum_{i=L}^{\infty} \mu \left(\frac{1-\mu^2}{4}\right)^{MN+i} \binom{2(MN+i)}{MN+i}$$

$$\times \left[1 - \sum_{n=0}^i \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right]. \quad (99)$$

Given the fact that

$$4^{-MN-i} \binom{2(MN+i)}{MN+i} < 1 \quad (100)$$

for all i , we have

$$\begin{aligned}
 &\lambda \sum_{i=L}^{\infty} \mu \left(\frac{1-\mu^2}{4}\right)^{MN+i} \binom{2(MN+i)}{MN+i} \\
 &\times \left[1 - \sum_{n=0}^i \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right] < \lambda \mu \sum_{i=L}^{\infty} (1-\mu^2)^{MN+i} \\
 &\times \left[1 - \sum_{n=0}^L \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right]. \quad (101)
 \end{aligned}$$

The right-hand side of (94) can be simplified to

$$\begin{aligned}
 &\lambda \mu \sum_{i=L}^{\infty} (1-\mu^2)^{MN+i} \left[1 - \sum_{n=0}^L \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right] \\
 &= \lambda \mu \left[1 - \sum_{n=0}^L \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right] \\
 &\quad (1-\mu^2)^{MN+L} \sum_{i=0}^{\infty} (1-\mu^2)^i. \quad (102)
 \end{aligned}$$

Given that

$$\sum_{i=0}^{\infty} q^i = \frac{1}{1-q}, \quad -1 \leq q \leq 1, \quad (103)$$

(94) can be written as

$$\begin{aligned}
 &\lambda \sum_{i=L}^{\infty} \mu \left(\frac{1-\mu^2}{4}\right)^{MN+i} \binom{2(MN+i)}{MN+i} \\
 &\times \left[1 - \sum_{n=0}^i \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right] < \lambda \frac{(1-\mu^2)^{MN+L}}{\mu} \\
 &\times \left[1 - \sum_{n=0}^L \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right]. \quad (104)
 \end{aligned}$$

Thus, truncation of (68) to the first N terms will introduce an error

$$Error = \lambda \left[1 - \sum_{n=0}^L \frac{(MNK)^n \exp\{-MNK\}}{\Gamma(n+1)} \right] (1-\mu^2)^{MN+L} \quad (105)$$

in the error probability.

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