MHD Visco-Elastic Fluid Flow and Heat Transfer
Around a Circular Cylinder

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Abstract:- An investigation is made on the temperature distribution within the thermal boundary layer region due to the flow of a second-grade fluid around a heated circular cylinder, maintained at a constant temperature higher than that of the fluid at infinity in presence of magnetic field applied transversely to the direction of the main flow. The problem has been solved by the application of steepest descent method used by Meksyn. The impact of various pertinent parameters on flow characteristics have been discussed through graphical illustrations. Newtonian results are found to emerge as limiting cases of the present analysis.

Key-words:- Visco-elastic, Boundary layer, MHD, Circular Cylinder, Heat transfer.

1 Introduction

The boundary layer concept has tremendous achievement in the interdisciplinary activities concerning engineering and technology developments. The mechanism of thermal boundary layer flow of magnetohydrodynamic visco-elastic fluids are used in different manufacturing processes such as extrusion of plastic sheets, fabrication of adhesive tapes, coating layers into rigid surfaces etc.

The influence of magnetic field on an electrically conducting viscous incompressible fluid past a cylinder in presence of heat transfer has practical significance in many engineering applications viz. solar power collectors, compact heat exchanges and nuclear reactors. Dennis and Chang [1] have presented the numerical solutions for steady flow past a circular cylinder at Reynolds numbers up to 100. An experimental investigation of the steady separated flow past a circular cylinder has been studied by Grove et al. [2]. Fornberg [3] has analysed the numerical study of steady viscous flow past a circular cylinder. Steady two-dimensional viscous flow of an incompressible fluid past a Circular cylinder has been investigated by Takami and Keller [4]. Also, the authors viz. Thoman and Szewczyk [5], Kawaguti [6], Hamielec and Raa1 [7], Gschwendter [8], Sen et al. [9] etc. have remarkable contribution in this field.

The study of visco-elastic fluid flow has been the objective of immense research due to its applications in industries of chemical processes such as food processing and polymer production etc. The differential models of visco-elastic fluid encountering the effects of shear thinning/thickening and normal stress differences are known as second-grade fluids which follow from generalized Rivlin-Ericksen’s fluid. The viscous feature of second-grade fluid is caused by the transport phenomenon of the molecules of fluids whereas the elastic characteristic is assignable to the chemical structure and configuration of polymer molecules. Many scientists have contribution on this field but a few of them are mentioned here. The second-order thermal boundary layer equation for the flow of a second-order fluid past heated body has been investigated by Srivastava [10] using the order of magnitude approach. The temperature distribution for the flow near a two-dimensional stagnation point occurring on a flat plate maintained at a temperature higher than that of the fluid at infinity has been analysed. The thermal boundary layer on a steadily rotating sphere in infinitely extending second-order fluid has been discussed by Bhakti and Palekar [11]. Srivastava and Maiti [12] have analysed the flow of a second-order fluid past a cylinder by expanding the flow functions in series and obtaining the first four terms by Karman-Pohlhausen method. The heat transfer in a second-grade fluid for flow around a
circular cylinder by Karman-Pohlhausen method has been studied by Srivastava and Saroa [13]. The heat transfer in the boundary layer region of a second-order fluid past a plate by presenting a uniform constant suction and temperature at the plate has been studied by Agarwal and Bhatia [14]. Srivastava and Saroa [15] have investigated the heat transfer in a second-order fluid past a circular cylinder in presence of magnetic field by numerical simulation of visco-elastic flow and heat transfer of a second-order fluid around a circular cylinder. Numerical study. Srivastava et al. [17] has presented the steady non-Newtonian flow past a circular cylinder: a numerical study.

In this paper, we have studied the problem of flow and heat transfer of a second-order fluid around a circular cylinder in presence of magnetic field by series expansion used by Meksyn [18] and found that the point of separation for the Newtonian case comes out to be 109.09° whereas the exact value is 109.6° [Schlichting,[19]]. Srivastava and Saroa [14] have obtained the separation point at 110.8° by taking the boundary layer thickness to be variable along the cylinder. By using Karman-Pohlhausen method, Srivastava and Maiti obtained the corresponding point of separation at 116.5°.

The constitutive equation for the second-order incompressible fluid is taken in the form

$$\sigma = -P I + \mu_1 A_1 + \mu_2 (A_1^2 + 2A_2) + \mu_3 A_1^2 $$ \hspace{1cm} (1)

where $\sigma$ is the stress tensor, $A_n (n = 1, 2)$ are the kinematic Rivlin-Ericksen tensors, $\mu_n (n = 1, 2, 3)$ are the material co-efficients describing the viscosity, elasticity and cross viscosity respectively. The case $\mu_2 = \mu_3 = 0$ corresponds to an incompressible Newtonian fluid. On thermodynamic considerations $\mu_2$ is found to be negative whereas $\mu_1$ and $\mu_3$ are positive. Coleman and Noll [20] derived the equation from the simple fluid by assuming that stress is more sensitive to the recent deformation than to the deformation that occurred in the distant past. Markovitz and Brown determined experimentally the material constants for solutions of poly-isobutylene in cetane of various concentrations.

2 Basic Equations

Consider an incompressible MHD second-grade fluid moving with a uniform velocity $U_\infty$ at infinity in presence of a fixed circular cylinder of radius $a$ maintained at a constant temperature $T_w$. Let the temperature of the fluid at infinity be $T_\infty$ where $T_w > T_\infty$. Let $(r, \theta, z)$ be the cylindrical polar co-ordinates with $z$-axis coincides with the axis of the cylinder. The fluid flow is two-dimensional in $r$ and $\theta$ directions.

The two-dimensional velocity boundary layer equations are

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu_1 \frac{\partial^2 u}{\partial y^2} + \nu_2 \left( \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} + \frac{\partial u}{\partial y} \frac{\partial^2 v}{\partial y^2} \right) + \frac{\sigma B_y^2}{\rho} (U - u) + U \frac{\partial u}{\partial x} $$ \hspace{1cm} (2)

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 $$ \hspace{1cm} (3)

where $y = r - a, x = a \theta$ and $u, v$ are velocity components along $x$ and $y$-axis respectively within the viscous boundary layer region, $U$ is the main stream velocity, $\rho$ is the fluid density, $B_y$ is the strength of the magnetic field and $\nu_i = \frac{\mu_i}{\rho}, (i = 1, 2)$.

Also, equations (2) and (3) are independent of the curvature of the wall and thus are applicable to the case of a flat wall.

Srivastava [1967] has derived the thermal boundary layer equation for the second-grade incompressible fluid against a heated wall as:

$$\rho C_p \left( \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) = \mu_1 \left( \frac{\partial u}{\partial y} \right)^2 + \mu_2 \left( v \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial y^2} + \frac{\partial u}{\partial y} \frac{\partial^2 v}{\partial y^2} \right) + k \frac{\partial^2 T}{\partial y^2} $$ \hspace{1cm} (4)

where $C_p$ is the specific heat, $k$ is the thermal conductivity and $T$ is the temperature. This equation is valid within the boundary layer over both a curved wall and a flat wall when $x$-axis is taken in the tangential direction and $y$-axis along the normal to the surface.

The relevant boundary conditions are,

$$u = 0, v = 0, T = T_w \text{ at } y = 0 $$ \hspace{1cm} (5)

$$u \rightarrow U, T \rightarrow T_\infty \text{ in } y \rightarrow \infty $$ \hspace{1cm} (6)

The velocity distribution $U$ outside the velocity boundary layer region created by the cylinder is given by,

$$U(\theta) = 2U_\infty \sin \theta $$

and the stream-function $\psi$ is given by,

$$\psi = \sqrt{\frac{\nu_2}{2U_\infty}} \left\{ 2U_\infty \theta f_1(\eta) - \frac{8}{3!} U_\infty \theta^3 f_3(\eta) + \frac{12}{5!} U_\infty \theta^5 f_5(\eta) - \frac{16}{7!} U_\infty \theta^7 f_7(\eta) + \cdots \right\} $$ \hspace{1cm} (7)
\[ \frac{\partial \psi}{\partial y} = 2 U_\infty \theta \left\{ f'_1(\eta) - \frac{2}{3} \theta^2 f_3'(\eta) + \frac{1}{20} \theta^4 f_5'(\eta) - \frac{1}{630} \theta^6 f_7'(\eta) + \cdots \right\} \]
\[ \frac{1}{4} \theta^4 f_5'(\eta) - \frac{1}{90} \theta^6 f_7'(\eta) + \cdots \]

where \( \eta = \sqrt{\frac{2U_\infty}{v_1}} \).

Now, the velocity components \( u \) and \( v \) within the velocity boundary layer region are given by,

\[ u = \frac{\partial \psi}{\partial y} = 2 U_\infty \theta \left\{ f'_1(\eta) - \frac{2}{3} \theta^2 f_3'(\eta) + \frac{1}{20} \theta^4 f_5'(\eta) - \frac{1}{630} \theta^6 f_7'(\eta) + \cdots \right\} \]
\[ \frac{1}{4} \theta^4 f_5'(\eta) - \frac{1}{90} \theta^6 f_7'(\eta) + \cdots \] (8)

and \[ v = -\frac{\partial \psi}{\partial x} = -\sqrt{\frac{2v_1 U_\infty}{a}} \left\{ f_1(\eta) - 2 \theta^2 f_3(\eta) + \frac{1}{12} \theta^4 f_5(\eta) - \frac{1}{90} \theta^6 f_7(\eta) + \cdots \right\} \] (9)

Here prime denotes differentiation w.r.t \( \eta \). The temperature \( T \) within the thermal boundary layer region should be taken in the form

\[ T' = \frac{T'_{\infty}}{T_{\infty}-T_{\infty}} = 4E \left\{ T_1(\eta) - \theta^2 T_3(\eta) + \theta^4 T_5(\eta) - \theta^6 T_7(\eta) + \cdots \right\} \]
\[ \frac{1}{4} \theta^4 f_5'(\eta) - \frac{1}{90} \theta^6 f_7'(\eta) + \cdots \] (10)

where \( E \) is the Eckert number and it is given by \( E = \frac{\mu_0^2}{C_p(\theta_{\infty} - \theta_{\infty})} \). For simplicity, we shall confine ourselves to terms up to \( f_5(\eta) \) and \( T_7(\eta) \) only.

Now, the boundary conditions of \( f_i(\eta) \) and \( T_i(\eta), (i = 1, 3, 5, 7) \) are,

At \( \eta = 0; f'_1(\eta) = 0, f'_3(\eta) = 0, T_1 = \frac{1}{4E}, T_3 = T_5 = T_7 = 0 \) (11)

In \( \eta \to \infty; f'_1 \to 1, f'_3 \to \frac{1}{4}, f'_5 \to \frac{1}{6}, f'_7 \to \frac{1}{8}, T_i \to 0 \) (12)

Now, substituting the values of \( u, v \) and \( T \) from equations (8) to (10) into (2) and (4) and equating the co-efficient of like powers of \( \theta \) with the neglect of higher order terms on both sides of the equations we have,

\[ f''_1 + f''_1 f''_1'' = -1 + M \left( f'_3 - 1 \right) + f''_1 + \alpha_1 \left( f''_1 + f''_3 f''_1'' - 2 f''_3 f''_1'' \right) \] (13)

\[ f''_3 + f''_3 f''_3'' = -1 + M \left( f'_3 - \frac{1}{3} \right) + 4 f'_3 f''_3 + 3 f''_1 f''_3'' + \alpha_1 \left( -4 f'_1 f''_1'' + f''_3 f''_1'' + 4 f''_3 f''_3'' + \left( f''_1 f''_3 + f''_3 f''_1'' \right) \right) \] (14)

\[ f''_5 + f''_5 f''_5'' = -\frac{8}{3} + M \left( f'_3 - \frac{1}{3} \right) + 6 f'_5 f''_5 - \frac{50}{3} f''_1 f''_5'' + \frac{80}{3} \left( f''_5 f''_5'' + f''_1 f''_3'' + f''_3 f''_1'' + \left( f''_1 f''_3'' + f''_3 f''_1'' \right) \right) \] (15)

\[ f''_7 + f''_7 f''_7'' = -8 + M \left( f'_7 - \frac{1}{8} \right) + 8 f'_7 f''_7 + 7 f''_1 f''_7'' + 168 f'_3 f''_3 + 63 f'_5 f''_5 + 105 f'_5 f''_7 + \alpha_1 \left( -8 f'_1 f''_1'' + f''_7 f''_7'' \right) \] (16)

\[ f''_1 + f''_1 f''_1'' = \frac{1}{4} \left( f''_1 + 3 f''_3 f''_1'' + 6 f''_5 f''_1'' - 80 f''_3 f''_1'' - 3 f''_3 f''_3'' \right) \] (17)

\[ f''_3 + f''_3 f''_3'' = \frac{1}{4} \left( f''_3 + 3 f''_3 f''_1'' + 6 f''_5 f''_3'' - 80 f''_3 f''_3'' - 3 f''_3 f''_3'' \right) \] (18)

\[ f''_5 + f''_5 f''_5'' = \frac{1}{4} \left( f''_5 + 3 f''_3 f''_5'' + 6 f''_5 f''_5'' - 80 f''_3 f''_5'' - 3 f''_3 f''_3'' \right) \] (19)

\[ f''_7 + f''_7 f''_7'' = \frac{1}{4} \left( f''_7 + 3 f''_3 f''_7'' + 6 f''_5 f''_7'' - 80 f''_3 f''_7'' - 3 f''_3 f''_3'' \right) \] (20)

where \( \alpha_1 = \frac{2 U_\infty v_1}{a} \) is the visco-elastic parameter, \( P_r = \frac{\rho v_1 C_p}{k} \) is the Prandtl number and \( M = \frac{\sigma B^2 u}{2 U_\infty \rho} \) is the magnetic parameter.

### 3 Solution of the Problem

The equations (13) to (20) subject to the boundary conditions (11) and (12) have been solved by the application of steepest decent method used by Meksyn followed by the method of Laplace. In this method we express the functions \( f_i(\eta) \) and \( T_i(\eta) \) in power series of \( \eta \) as

\[ f_i(\eta) = A_i \eta^2 + B_i \eta^3 + C_i \eta^4 + D_i \eta^5 + E_i \eta^6 + \cdots \] (21)

\[ T_i(\eta) = \frac{1}{4E} + a_i \eta + b_i \eta^2 + c_i \eta^3 + d_i \eta^4 + e_i \eta^5 + \cdots \] (22)

where \( A_i, B_i, C_i, D_i, E_i, a_i, b_i, c_i, d_i, e_i \) are the constants to be determined which can be obtained by solving the system of equations (13) to (20) subject to the boundary conditions (11) and (12).
\[ T_j(\eta) = a_j \eta + \frac{b_j}{2!} \eta^2 + \frac{c_j}{3!} \eta^3 + \frac{d_j}{4!} \eta^4 + \frac{e_j}{5!} \eta^5 + \ldots \]  

(23)

where \( i = 1,3,5,7 \) and \( j = 3,5,7 \).

We have taken the above forms of \( f_i, T_1 \) and \( T_j \) for sufficiently small values of \( \eta \) and all of them satisfy the boundary conditions (11) at \( \eta = 0 \). Now substituting the expressions of \( f_i, T_1 \) and \( T_j \) from (21), (22) and (23) into (13) to (20) and equating the co-efficient of different powers of \( \eta \) to zero, we obtain the constants \( A_i \)'s and \( a_i \)'s only. So, if \( A_i \) and \( a_i \) are known, the velocity and the temperature distributions are completely determined.

Now we write equations (13) to (16) and (17) to (20) in the following forms:

\[ f_i''' + f_i f_i'' = H_i(\eta), \; i = 1,3,5,7 \]  

(24)

and

\[ T_i''' + Pr f_i T_i' = M_i(\eta), \; i = 1,3,5,7 \]  

(25)

Here we have denoted the right-hand sides of the equations (13) to (16) and (17) to (20) by \( H_i(\eta) \) and \( M_i(\eta) \) respectively. Now integrating twice the equations (24) and (25) w.r.t \( \eta \) from 0 to \( \eta \), we get

\[ f_i'(\eta) = \int_0^\eta e^{-F(\eta)} \phi_i(\eta) \, d\eta \]  

(26)

\[ T_i(\eta) = a_0 + \int_0^\eta e^{-G(\eta)} \psi_i(\eta) \, d\eta \]  

(27)

where

\[ F(\eta) = \int_0^\eta f_1(\eta) \, d\eta \]

\[ G(\eta) = Pr \int_0^\eta f_1(\eta) \, d\eta \]

\[ \phi_i(\eta) = A_i + \int_0^\eta e^{F(\eta)} H_i(\eta) \, d\eta \]

\[ \psi_i(\eta) = a_i + \int_0^\eta e^{G(\eta)} M_i(\eta) \, d\eta \]

Now, taking \( \eta \to \infty \) in the equations (26) and (27) we get,

\[ \int_0^\infty e^{-F(\eta)} \phi_i(\eta) \, d\eta = 1 \]

\[ \int_0^\infty e^{-F(\eta)} \psi_3(\eta) \, d\eta = \frac{1}{4} \]

\[ \int_0^\infty e^{-F(\eta)} \psi_5(\eta) \, d\eta = \frac{1}{6} \]

\[ \int_0^\infty e^{-F(\eta)} \psi_7(\eta) \, d\eta = \frac{1}{8} \]  

(28)

and

\[
\begin{align*}
\int_0^\infty e^{-G(\eta)} \psi_1(\eta) \, d\eta &= -\frac{1}{4E} \\
\int_0^\infty e^{-G(\eta)} \psi_3(\eta) \, d\eta &= 0 \\
\int_0^\infty e^{-G(\eta)} \psi_5(\eta) \, d\eta &= 0 \\
\int_0^\infty e^{-G(\eta)} \psi_7(\eta) \, d\eta &= 0
\end{align*}
\]  

(29)

The above integrals can be evaluated asymptotically by Laplace’s method. Putting \( F(\eta) = G(\eta) = \delta \), transforming the equations (28) and (29) to the variable \( \delta \) and integrating in the gamma functions, we have,

\[
\begin{align*}
m_{10} \Gamma_1 + m_{11} \Gamma_2 + m_{12} \Gamma_4 + m_{13} \Gamma_5 + m_{14} \Gamma_5 + \ldots &= 1 \\
m_{30} \Gamma_3 + m_{31} \Gamma_4 + m_{32} \Gamma_1 + m_{33} \Gamma_4 + m_{34} \Gamma_5 + \ldots &= \frac{1}{4} \\
m_{50} \Gamma_5 + m_{51} \Gamma_2 + m_{52} \Gamma_1 + m_{53} \Gamma_4 + m_{54} \Gamma_5 + \ldots &= \frac{1}{6} \\
m_{70} \Gamma_5 + m_{71} \Gamma_2 + m_{72} \Gamma_1 + m_{73} \Gamma_4 + m_{74} \Gamma_5 + \ldots &= \frac{1}{8}
\end{align*}
\]  

(30)

\[
\begin{align*}
n_{10} \Gamma_1 + n_{11} \Gamma_2 + n_{12} \Gamma_4 + n_{13} \Gamma_5 + n_{14} \Gamma_5 + \ldots &= -\frac{1}{4E} \\
n_{30} \Gamma_3 + n_{31} \Gamma_4 + n_{32} \Gamma_1 + n_{33} \Gamma_4 + n_{34} \Gamma_5 + \ldots &= 0 \\
n_{50} \Gamma_5 + n_{51} \Gamma_2 + n_{52} \Gamma_1 + n_{53} \Gamma_4 + n_{54} \Gamma_5 + \ldots &= 0 \\
n_{70} \Gamma_5 + n_{71} \Gamma_2 + n_{72} \Gamma_1 + n_{73} \Gamma_4 + n_{74} \Gamma_5 + \ldots &= 0
\end{align*}
\]  

(31)

where the constants are not presented here due to sake of brevity. Now solving the equations (30) and (31) using MATLAB, we get the values of \( A_i \)'s and \( a_i \)'s (\( i = 1,3,5,7 \)) for different flow parameters involved in the equations (Tables 1 to 5). Throughout the computations, we use different values of magnetic parameter \( M \), Prandtl number \( Pr \).
and visco-elastic parameter $\alpha_1$ with fixed value of Eckert number $E = 0.1$. In the study, the Newtonian fluid flow phenomenon is illustrated by $\alpha_1 = 0$ and $\alpha_1 \neq 0$ characterizes the visco-elastic fluid. Now using the values of $A_j's$ and $\alpha_i's$ in equations (21) to (23), we get the expressions for $f_1, T_1$ and $T_j$. Finally putting the values of $f_1, T_1$ and $T_j$ in equations (8) to (10) we get the analytical expressions for velocity components $u, v$ within the velocity boundary region and temperature $T^*$ within the thermal boundary layer region.

### 4 Results and Discussion

Knowing the velocity and temperature fields, we obtain some important flow characteristics of the problem viz. wall shear stress and local heat flux.

The non-dimensional shearing stress $\tau$ at the wall $\eta = 0$ is given by,

$$
\tau = \frac{\sigma_{xy}}{2 \rho U_\infty} = \left\{ \theta f_{1''}(\eta) - \frac{4}{31} \theta^3 f_3(\eta) + \frac{6}{31} \theta^5 f_2''(\eta) - \frac{8}{71} \theta^7 f_1''(\eta) + \ldots \right\}_{\eta = 0}
$$

Equations (33), (34) and (35) are $X = 3.6218, X = 3.2282$ and $X = 2.6753$ respectively. Thus the points of separation for $\alpha_1 = 0, -0.01, and -0.03$ occur at $\theta = 109.09^\circ, \theta = 102.99^\circ$ and $\theta = 93.76^\circ$ respectively. Thus, we observe that the separation point diminishes with the enhancement of absolute value of visco-elastic parameter. Again, if we increase the value of magnetic parameter, ($M = 0.15$) then we get the separation point for $\alpha_1 = 0, -0.01,$ and $-0.03$ at $\theta = 111.09^\circ, \theta = 104.32^\circ$ and $\theta = 94.42^\circ$ respectively. So, it can be remarked that the enhancement of magnetic parameter increases the value of separation point in both Newtonian and non-Newtonian cases.

The heat generation flux $g$ from the cylinder to the fluid is given by,

$$
g = -k \left( \frac{\partial T}{\partial y} \right)_{y=0} = -\frac{4 k E \sqrt{R e}}{a} (T_w - T_\infty) (T_1' (\eta) - \theta^2 T_3'(\eta) + \theta^4 T_5'(\eta) - \theta^6 T_7'(\eta))_{\eta=0}
$$

where $Re = \frac{2 U_\infty \rho}{\mu_1}$ is the Reynolds number.

Defining the Nusselt number $Nu = \frac{ag}{k(T_w - T_\infty)}$ we have,

$$
Nu = -4 E \sqrt{R e} (T_1' (\eta) - \theta^2 T_3'(\eta) + \theta^4 T_5'(\eta) - \theta^6 T_7'(\eta))_{\eta=0}
$$

Figures 1 to 5 demonstrate the variation of shearing stress $\tau$ and $\frac{Nu}{\sqrt{Re}}$ against $\theta$ with various values of other flow parameters. The various angles (in degrees) are converted in radians (1 = 0.0175 radian) while plotting the graphs in different cases.

The graphs reveal that the shearing stress $\tau$ and $\frac{Nu}{\sqrt{Re}}$ gradually diminish for Newtonian and non-Newtonian fluids. Also, it is observed that the growth of absolute value of visco-elastic parameter $\alpha_1$, decelerate the shearing stress $\tau$ and $\frac{Nu}{\sqrt{Re}}$ in comparison with Newtonian fluid flow phenomenon. The rising values of magnetic parameter $M$ accelerate the shearing stress for both types of fluids (Figures 1 and 2). Again from the figures 3, 4 and 5, it can be revealed that the growth of magnetic parameter increases $\frac{Nu}{\sqrt{Re}}$ but an opposite trend is demonstrated during the growing behaviour of Prandtl number $Pr$. It has been observed that the Meksyn method is useful and depicts better result when skin friction, heat flux etc. are calculated at the wall of the solid body.

### 5 Conclusion

The flow and heat transfer of a visco-elastic fluid around a circular cylinder in presence of a magnetic field has been analysed using the application of steepest descent method used by Meksyn. This study leads to the following conclusions:

- The velocity and temperature fields are significantly affected by visco-elasticity.
• The point of separation for Newtonian case comes to be $109.09^\circ$ whereas the exact value is $109.6^\circ$.
• The point of separation has been found to shift towards the forward stagnation point due to the elasticity of the fluid.
• The enhancement of the value of separation point is noticed for both Newtonian and visco-elastic fluids with the increasing value of magnetic parameter.
• With the growth of the absolute value of the visco-elastic parameter, the shearing stress diminishes and the identical result is seen for Nusselt number.
• Both the shearing stress and Nusselt number show diminishing trends with the increase of the angle $\theta$ in both types of fluids.

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References


Fig. 1 Variation of $\tau$ against $\theta$ for $M = 0.08$.

Fig. 2 Variation of $\tau$ against $\theta$ for $M = 0.15$. 
Fig. 3  Variation of $\frac{Nu}{\sqrt{Re}}$ against $\theta$ for $M = 0.08$, $Pr = 3$, $E = 0.1$.

Fig. 4  Variation of $\frac{Nu}{\sqrt{Re}}$ against $\theta$ for $M = 0.15$, $Pr = 3$, $E = 0.1$.

Fig. 5  Variation of $\frac{Nu}{\sqrt{Re}}$ against $\theta$ for $M = 0.08$, $Pr = 5$, $E = 0.1$. 
Table 1. Values of $A_i$ ($i = 1, 3, 5, 7$) at $M = 0.08$

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Table 2. Values of $A_i$ ($i = 1, 3, 5, 7$) at $M = 0.15$.

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</tr>
</tbody>
</table>

Table 3. Values of $a_i$ ($i = 1, 3, 5, 7$) at $M = 0.08$, $Pr = 3$ and $E = 0.1$. 
<table>
<thead>
<tr>
<th>$a_1$</th>
<th>0</th>
<th>-0.01</th>
<th>-0.03</th>
</tr>
</thead>
<tbody>
<tr>
<td>$a_1$</td>
<td>-0.0167</td>
<td>-0.0167</td>
<td>-0.0167</td>
</tr>
<tr>
<td>$a_3$</td>
<td>-0.8783</td>
<td>-0.8825</td>
<td>-0.891</td>
</tr>
<tr>
<td>$a_5$</td>
<td>-1.3362</td>
<td>-1.3544</td>
<td>-1.3928</td>
</tr>
<tr>
<td>$a_7$</td>
<td>-1.7736</td>
<td>-1.8257</td>
<td>-1.9417</td>
</tr>
</tbody>
</table>

Table 4. Values of $a_i$ ($i = 1,3,5,7$) at $M = 0.15, Pr = 3$ and $E = 0.1$

<table>
<thead>
<tr>
<th>$a_1$</th>
<th>0</th>
<th>-0.01</th>
<th>-0.03</th>
</tr>
</thead>
<tbody>
<tr>
<td>$a_1$</td>
<td>-0.0257</td>
<td>-0.0257</td>
<td>-0.0257</td>
</tr>
<tr>
<td>$a_3$</td>
<td>-1.0603</td>
<td>-1.0641</td>
<td>-1.0715</td>
</tr>
<tr>
<td>$a_5$</td>
<td>-2.021</td>
<td>-2.0518</td>
<td>-2.1195</td>
</tr>
<tr>
<td>$a_7$</td>
<td>-2.4416</td>
<td>-2.5225</td>
<td>-2.7049</td>
</tr>
</tbody>
</table>

Table 5. Values of $a_i$ ($i = 1,3,5,7$) at $M = 0.08, Pr = 5$ and $E = 0.1$. 